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- (1) Program Number (to be filled in by SPLA)..... 360D-17.4.005
- (2) System Type (machine)..... S/360, S/370
- (3) Search Key.....

- (4) Programming Systems/Languages..... FORTRAN
- (5) Author's Name and Address..... H.M. Selim and J.M. Davidson
Soil Science Department
G-169 McCarty Hall; University of Florida
- (6) Direct Technical Inquiries to Name & Address Gainesville, Florida 32611
(if different than Author)

- (7) Title of Program..... Numerical solution of nitrogen transformations and
transport equations during transient unsaturated water
flow in soils

- (8) Submitter's Installation Membership Code..... UF
- (9) Submitter's Own Program Identification and Suffix(Optional)..

- (10) Primary Subject Code..... 17 4
- (11) Minimum System Requirements 128K
- (12) New or Revision Code (if revision, show prior Program Number in Item 1) N
- (13) Year Completed..... 1976
- (14) Date of Submittal..... 10/06/76
- (15) Documentation (number of original pages submitted)..... 53
- (16) Abstract (should contain sufficient information for a reader to determine the value of the program). Listed on the reverse side of this form are subjects which may serve as a guide for a descriptive abstract.

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Subject Guide:

- a. Purpose
- b. Programming Language used
- c. Version and modification level or release number
- d. Field of application
- e. Type of routine (main program, subroutine, etc.)
- f. Specific description of machine requirements

ABSTRACT

A numerical solution is presented for the partial differential equations governing nitrogen transformations and transport under conditions of transient unsaturated water flow in soils. Nitrogen species considered were: NH_4 and NO_3 in soil solution, exchangeable NH_4 , organic-N, and gaseous N. The solution is based on finite-difference approximations (explicit-implicit) of the transient soil water flow equation and the convective-dispersive equations for transport of NH_4 and NO_3 along with the nitrogen transformation equations. The transformation equations incorporated in the model describe nitrification, denitrification, mineralization, immobilization, and ion-exchange process. The ion-exchange process was considered to be instantaneous whereas all transformation processes were of first-order kinetic type. The boundary conditions at the soil surface include a continuous NH_4 and/or NO_3 flux and water infiltration under constant head. The initial conditions include uniform as well as nonuniform initial nitrogen and water content distributions throughout the soil profile.

The computer program is written in FORTRAN language and consists of a source program, seventeen subprograms and an input data section. The program also utilizes the GOULD plotter to generate plots of water content, NH_4 , NO_3 and organic-N versus soil depths for specified times desired. An important feature of the program is that incremental distances and time steps are automatically adjusted to satisfy the stability criteria for the water and nitrogen finite difference equations. The program is flexible and can be adjusted to incorporate nonhomogeneous soils and variable nitrogen transformation rate coefficients with water and soil depths as desired.

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 EBCDIC
 Sequence 00000010 through 00008830 in cols. 73-80;
 883 cards
 883 card images blocked 20 per block
 44 blocks of 1600 characters each and 1 block of
 240 characters

T/M

File 2 Sample Data Input
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 No sequencing; 22 cards
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NUMERICAL SOLUTION OF NITROGEN TRANSFORMATIONS AND
TRANSPORT EQUATIONS DURING TRANSIENT UNSATURATED WATER FLOW IN SOILS

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Gainesville, Florida 32611

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A numerical solution which is based on finite difference methods is presented for the problem of nitrogen transformations and transport during transient water flow in soils. The nonlinear partial differential equation governing one-dimensional flow of water in unsaturated soils may be written as (see Kirkham and Powers, 1972, Selim et al. 1976),

$$\text{Cap}(h) \frac{\partial h}{\partial t} = \frac{\partial}{\partial z} K(h) \frac{\partial h}{\partial z} - \frac{\partial K(h)}{\partial z} \quad (1)$$

where

θ = soil water content (cm^3/cm^3),

h = soil water head or suction (cm),

$K(h)$ = soil hydraulic conductivity (cm/hr),

z = distance in soil, positive downward (cm),

t = time.

$\text{Cap}(h)$ = soil water capacity (cm^{-1}).

In equation (1) the soil water capacity $\text{Cap}(h)$ is a measure of the change of soil water content with water head ($\text{Cap}(h) = \partial\theta/\partial h$) which is determined using soil water characteristic relationships (θ versus h).

Nitrogen transformations and transport were considered for the following nitrogen species, NH_4 and NO_3 in soil solution, exchangeable NH_4 , organic-N, and gaseous-N. Only NH_4 and NO_3 in soil solution was considered mobile and were thus described by the convective-dispersive solute transport equations (Selim et al. 1976). Nitrogen transformation process incorporated in the model were nitrification, denitrification, mineralization, immobilization, and ion-exchange.

The ion-exchange process was considered to be instantaneous whereas all transformation processes were of first-order kinetic type.

The equations governing the transport and transformations of NH_4 and NO_3 in soil solution may be expressed as (Misra et al. 1974)

$$R \frac{\partial A}{\partial t} = D \frac{\partial^2 A}{\partial z^2} - \frac{V}{\theta} \frac{\partial A}{\partial z} - k_1 A - k_4 A + \frac{\rho}{\theta} k_3 O \quad (2)$$

and

$$\frac{\partial B}{\partial t} = D \frac{\partial^2 B}{\partial z^2} - \frac{V}{\theta} \frac{\partial B}{\partial z} + k_1 A - k_2 B - k_5 B \quad (3)$$

where A = concentration of NH_4 in soil solution (mg/cm^3),
 B = concentration of NO_3 in soil solution (mg/cm^3),
 E = amount of NH_4 in exchangeable phase per gram soil (mg/g),
 O = amount of N in organic phase (mg/g),
 G = amount of N_2O and/or N_2 gas produced per gram soil (mg/g),
 k_1, k_2, k_3, k_4, k_5 = kinetic rate coefficients, respectively, for NH_4 nitrification, NO_3 immobilization, NH_4 mineralization, immobilization of organic N , and NO_3 denitrification (hr^{-1}).
 D = dispersion coefficient (cm^2/hr),
 ρ = soil bulk density (g/cm^3),
 $V = q(z) - \theta \frac{\partial D}{\partial z} - D \frac{\partial \theta}{\partial z}$, where $q(z)$ is the Darcy water flux (cm/hr),
 k_D = distribution coefficient of NH_4 in the exchangeable phase (cm^3/g),
 $R = 1 + \rho k_D / \theta$, retardation factor for NH_4 exchangeable.

The first two terms of the right side of (2) and (3) account for solute transport. These two terms are usually referred to as the dispersion and mass flow terms, respectively. The third, fourth, and fifth terms of equation (2) represent NH_4 nitrification, immobilization, and mineralization processes, respectively. Similarly, the last three terms of equation (3) represent nitrification, immobilization of NO_3 , and denitrification, respectively.

The ion-exchange process governing NH_4 adsorption-desorption may be expressed as,

$$E = k_D A \quad (4)$$

The transformations of organic N and denitrification processes, respectively, are

$$\rho \frac{\partial O}{\partial t} = k_2 \theta B + k_4 \theta A - k_3 \rho O \quad (5)$$

and

$$\rho \frac{\partial G}{\partial t} = k_5 \theta B \quad (6)$$

In equation (2) to (6), the reaction between NH_4 in soil solution (A) and that exchangeable (E) is assumed instantaneous whereas all other transformations are considered to be first-order kinetic reactions.

The initial conditions used are nonuniform water content and nitrogen concentration distributions in a semi-infinite soil column,

$$h = h(z, 0), \quad 0 < z < \infty \quad (7)$$

$$A = A(z, 0), \quad 0 < z < \infty \quad (8)$$

$$B = B(z, 0), \quad 0 < z < \infty \quad (9)$$

$$O = O(z, 0), \quad 0 < z < \infty \quad (10)$$

For the water flow equation (1), the boundary condition at the soil surface ($z=0$) is a constant (or variable) water head H ,

$$h = H, \quad z = 0, \quad t \leq t_1 \quad (11)$$

which describes continuous water infiltration for length of time t_1 . Following water infiltration, i.e. for times greater than t_1 , the boundary condition is,

$$q_{z=0} = -K(h) \frac{\partial h}{\partial z} + K(h), \quad z = 0, \quad t > t_1 \quad (12)$$

Equation (12) describes water redistribution under a constant (or variable) evapoative water flux $q_{z=0}$ at the soil surface.

For the nitrogen transport and transformation equations (2) and (3), the boundary condition at $z=0$ is a continuous solute (NH_4 or NO_3) flux where

$$qA - \theta D \frac{\partial A}{\partial z} = q \text{ CI}, \quad z = 0, \quad t \leq t_2 \quad (13)$$

$$qB - \theta D \frac{\partial B}{\partial z} = q \text{ CII}, \quad z = 0, \quad t \leq t_2 \quad (14)$$

where CI and CII are concentrations of applied solutions of NH_4 and NO_3 , respectively. When application of these solute solutions is terminated (i.e. $t > t_2$), equations (13) and (14) are also used with CI and CII equal zero provided that $t_2 \leq t_1$.

Since the values of $K(h)$ and V in equations (1), (2) and (3) are not constant, these equations are nonlinear and cannot be solved analytically. In order to obtain a numerical solution for equations (1) to (6) subject to conditions (7) to (14), we express these equations in finite difference approximation forms. In this study, the explicit-implicite finite difference scheme (Carnahan et al., 1969; Salvadori and Baron, 1961) is used. We refer to a discrete set of points in the (z, t) plane given by a grid with spacings Δz and Δt , respectively. Grid or mesh points are denoted by (i, n) where

$$\begin{aligned} z &= i \Delta z, & i &= 1, 2, 3, \dots \\ t &= n \Delta t, & n &= 1, 2, 3, \dots \end{aligned}$$

The finite difference approximation for the water flow equation (1) is

$$\begin{aligned} \text{Cap}(h_i^{n+1/2}) [h_i^{n+1} - h_i^n] &= \gamma K(h_{i+1/2}^{n+1/2}) [h_{i+1}^{n+1} - h_i^{n+1}] \\ &\quad - \gamma K(h_{i-1/2}^{n+1/2}) [h_i^{n+1} - h_{i-1}^{n+1}] \\ &\quad + \gamma K(h_{i+1/2}^{n+1/2}) [h_{i+1}^n - h_i^n] \\ &\quad - \gamma K(h_{i-1/2}^{n+1/2}) [h_i^n - h_{i-1}^n] \\ &\quad - \beta [K(h_{i+1/2}^n) + K(h_{i-1/2}^n)] \end{aligned} \quad (15)$$

where $\gamma = \Delta t / 2(\Delta z)^2$ and $\beta = \Delta t / \Delta z$. Similarly, finite difference approximations for the equation governing NH_4 transport and transformation (equation 2) may be expressed as

$$\begin{aligned} R_i^{n+1} [A_i^{n+1} - A_i^n] &= \gamma D_i^{n+1/2} [A_{i+1}^{n+1} - 2 A_i^{n+1} + A_{i-1}^{n+1}] \\ &\quad + \gamma D_i^{n+1/2} [A_{i+1}^n - 2 A_i^n + A_{i-1}^n] \\ &\quad - (V/\theta)_i^{n+1} \beta [A_{i+1}^{n+1} - A_i^{n+1}] \\ &\quad - (k_1 + k_4) \Delta t A_i^n + k_3 (\rho/\theta) \Delta t O_i^n \end{aligned} \quad (16)$$

and the finite difference for equation (3) is

$$\begin{aligned}
 B_i^{n+1} - B_i^n &= \gamma D_i^{n+\frac{1}{2}} [B_{i+1}^{n+1} - 2 B_i^{n+1} + B_{i-1}^{n+1}] \\
 &- \gamma D_i^{n+\frac{1}{2}} [B_{i+1}^n - 2 B_i^n + B_{i-1}^n] \\
 &- (V/0)_i^{n+1} \beta [B_{i+1}^{n+1} - B_i^n] + k_1 \Delta t A_i^{n+1} \\
 &- (k_2 + k_5) \Delta t B_i^n.
 \end{aligned} \tag{17}$$

Equations (15), (16) and (17) are nonlinear since the values of $\text{Cap}(h_i^{n+\frac{1}{2}})$, $K(h_i^{n+\frac{1}{2}})$, $D_i^{n+\frac{1}{2}}$ are dependent on h_i^{n+1} for which solutions are being sought. The iteration method described by Remson et. al. (1971) is usually used to predict $h^{n+\frac{1}{2}}$ using h^n . Selim and Kirkham (1973) showed that the solution of the water flow equation can be approximated satisfactorily using h^n when smaller Δt than required for stable solution is used. This simplifies the computation considerably since the system of equations becomes linear. Accordingly, the following approximations were made

$$\text{Cap}(h_i^{n+\frac{1}{2}}) = \text{Cap}(h_i^n)$$

$$K(h_i^{n+\frac{1}{2}}) = K(h_i^n)$$

$$D_i^{n+\frac{1}{2}} = D_i^{n+\frac{1}{2}}$$

Incorporation of the initial and boundary conditions in their finite difference forms and rearrangement of equations (15), (16), and (17) yield three linear systems of equations. In matrix-vector form; each system of equations yield a tridiagonal real matrix associated with a real column vector. In absolute value, the coefficients of the main diagonal of each matrix is greater than the raw sum of the off-diagonal coefficients. Hence, the matrix for each system of equations is diagonally dominant (Varga, 1962, p. 23). Therefore, each matrix is nonsingular, and there exists a solution and the solution is unique.

To satisfy the convergence criteria in solving equations (15), (16), and (17), the increments Δz and Δt were chosen such that

$$\Delta z \leq D_{\max}/V_{\max}$$

$$\Delta t \leq \Delta z/2V_{\max}$$

$$\frac{\Delta t}{(\Delta z)^2} \left(\frac{K}{Cap_{\max}} \right) \leq 1/2$$

where D_{\max} , V_{\max} , K_{\max} , Cap_{\max} are the maximum values of D , V , K , and Cap at any time step.

So far we have presented numerical solutions for the water flow equation (1), and the NH_4 and NO_3 transport and transformation equations (2), and (3). In order to complete the nitrogen transformation processes, it is necessary to solve for the exchangeable NH_4 (E), organic-N (O), and gaseous-N (G) at every time step and incremental distance in the soil profile. This was achieved by solving equation (4), (5) and (6) as follows;

$$E_i^{n+1} = k_D C_i^{n+1}, \quad (18)$$

$$O_i^{n+1} = O_i^n + (\Delta t/\rho) [k_2 \theta B_i^{n+1} + k_4 \theta A_i^{n+1} - k_3 \rho O_i^n] \quad (19)$$

$$G_i^{n+1} = G_i^n + (\Delta t/\rho) k_5 \theta B_i^{n+1} \quad (20)$$

In the computer program, for any time step $n+1$, where all variables are assumed known at time step n , equations (15) to (20) are solved sequentially until a desired time t is reached.

DESCRIPTION OF THE COMPUTER PROGRAM

The computer program consists of a source program and seventeen subprograms, and an input data section. The names of the subprograms are AXISPL, GRAPH, CHECKT, WATER, MOISD, INITWT, SBCW, INITST, DADJ, DADJD, CHECKN, AMONIA, NITRAT, GASORG, OUTPUT, TINT, and TRIDM. The user of this program must provide parameters in the form of punched data cards in the data section, and as FORTRAN statements in the SBCW and WATER subprograms. The remaining source program and subprograms need not be altered and remain valid for all situations.

The main function of the main program is prescribing the DIMENSION and COMMON statements, and reading of input parameters, as well as setting up the entire sequence of the program. Subprograms INITWT, INITST, and MOISD provide the initial distributions of all the variables and calculates Δz and Δt according to the stability criteria. Subprogram SBCW provides h at $z=0$ according to the boundary conditions of the water flow equation, which may be altered by the user as desired. Subprograms WATER, AMONIA, and NITRAT provide the solution for water head (h), NH_4 concentration (A) and NO_3 concentration (B), respectively. Subprogram GASORG calculate the amount of organic-N and gaseous-N. Subprogram TRIDM provides the solution for a linear system of equations with a tridiagonal coefficient matrix.

The dispersion coefficient D and the hydraulic conductivity K are calculated at each time step in the WATER subprogram. Here, D and K are provided as a function of (q/θ) and θ , respectively, but may be changed as desired. In addition, $\text{Cap}(h)$ and conversion of h to θ at all incremental points in the soil profile were calculated in the WATER subprogram. This conversion is based on θ versus h relationship (in a tabular form) as given by the soil water characteristic of individual soils.

An important feature of the program is that increments of Δz and Δt are adjusted automatically to satisfy stability and convergence criteria for the

for the water and salt finite difference equations. These adjustments are carried out automatically every 20 time steps using subprograms DADJ and DADJD. Another program feature is that the number of nodal points (increments) are automatically calculated from the length of the flow region (soil column). Only that portion of the soil column where solute and water flow are currently taking place is considered. The adjustments of the number of nodal points are made using subprogram CHECKN. This number is checked every 20 time steps, and no further changes of the number of increments will occur when the total column length is reached. This feature minimizes the unnecessary use of a large number of nodal points and saves considerable amount of CPU time. A third feature of the program is that data are provided at specified times. This adjustment is carried out using subprogram CHECKT, where Δt 's are continuously adjusted until the prescribed times are reached. For each prescribed time; h , θ , K , q , $\text{NH}_4\text{-N}$, $\text{NO}_3\text{-N}$, organic-N, gaseous-N throughout the soil column are printed using subprogram OUTPUT. Subprograms AXTSPL and GRAPH provide plots (using GOULD plotter) for θ , NH_4 , NH_3 , and Org-N versus depth for a series of times as desired. The scale and length of each plot is prescribed in these subprograms and may be changed by the user.

PROGRAM PARAMETERS

The following parameters are inputs to be provided in the DATA section:

NX = number of data points of the soil water characteristic relationship
(θ versus h)

THC = water content θ from soil water characteristic relationship (dimension = NX)

HC = corresponding water head h from soil water characteristic relationship
(dimension = NX)

DZ = initial approximation for Δz

DT = initial approximation for Δt

DISP = initial approximations for dispersion coefficient D

THMIN = minimum soil water content (estimated)

THMAX = maximum soil water content

NT = number of prescribed times at which data and plots (using GOULD plotter) are desired.

TIT = times at which output and plots are desired (dimension = NT)

RKD = k_D (see equation 4)

RK1 = K_1 (see equations 2 to 6)

RK2 = k_2 (see equations 2 to 6)

RK3 = k_3 (see equations 2 to 6)

RK4 = k_4 (see equations 2 to 6)

RK5 = k_5 (see equations 2 to 6)

NTT = number of points for initial distributions of water and nitrogen species in the soil profile

XXX = depths at which initial distributions are given (dimension = NTT)

C1 = initial distribution of water head (h) in the soil profile (dimension = NTT)

C2 = initial distribution of water content (θ) in the soil profile (dimension = NTT)

C3 = initial distribution of NH_4 (dimension = NTT)

C4 = initial distribution of NO_3 (dimension = NTT)

C5 = initial distribution of organic-N (dimension = NTT)

C6 = initial distribution of gaseous-N (dimension = NTT)

ROU = ρ , soil bulk density

COLUMN = length of soil profile

TSALT = length of time of solute application

TWD = length of time of water infiltration

CONST = hydraulic conductivity at saturation

AC = a coefficient for K versus θ relationship

BC = a coefficient for K versus θ relationship

CSNH₄ = concentration of NH_4 in applied solution

CSNO₃ = concentration of NO_3 in applied solution

DFLUX = evaporative flux during water redistribution (time > TWD)

Input parameters to be provided in subprogram WATER are

CON = water hydraulic conductivity K

DISPC = dispersion coefficient D

Input parameter to be provided in subprogram SBCW is

H(1) = water head h at $z=0$ during infiltration and maximum h during redistribution

Other notations used in the program are

TH = soil water content, θ

H = water suction or head, h

CNH₄ = concentration of NH₄ in soil solution, A

CNO₃ = concentration of NO₃ in soil solution, B

CORGN = amount of organic-N per gram soil, O

CNO₂ = amount of gaseous-N per gram soil, G

CAP = soil water capacity, Cap(h)

WFLUX = soil water flux, q

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7. Selim, H. M., R. S. Mansell, and A. Elzeftawy. 1976. Distributions of 2,4-D and water in soil during infiltration and redistribution. Soil Sci. 121:176-183.
8. Varga, R. S. 1962. Matrix Iterative Analysis. Prentice Hall, New Jersey.

SAMPLE PROGRAM

The attached program listing, output, and GOULD plots are for water and nitrogen transport and transformation in a Norge loam soil profile. The example considered is for continuous water infiltration into a uniform profile for 10 hours. NH_4 and NO_3 were introduced with the infiltrating water for the first hour. The concentration of NH_4 as well as NO_3 was 100 mg/cm^3 . Initial water content θ , NH_4 , NO_3 , and organic N were considered uniform throughout the soil profile where,

$$\theta = 0.22 \text{ cm}^3/\text{cm}^3$$

$$h = -300.0 \text{ cm}$$

$$\text{NH}_4 = 0$$

$$\text{NO}_3 = 0$$

$$\text{Organic-N} = 20 \text{ mg/g.}$$

The hydraulic conductivity $K(h)$ used was in a functional form (see subprograms WATER),

$$K(h) = 1.8 \times 10^{-11} \times \exp(65.6\theta) \quad \text{cm/hr}$$

In addition, the θ versus h relation (or the water characteristic relation) was used to calculate $\text{Cap}(h)$. This θ versus h relation was given in a tabular form which is listed in the input section of the program.

In order to avoid the excessive costs which are commonly generated when the water boundary condition $h=0$ at $z=0$ is imposed at the early stages of wetting, the following boundary condition was used. At the beginning of water infiltration h was set equal to -100 cm rather than zero. At each incremental time step h was then increased by a constant increment of 0.4 (see subprogram SBCW). No further change of h was allowed when h became zero. For the example attached, the total time required for h to reach zero was 0.0484 hr .

Other parameters include:

soil bulk density, ρ 1.6 g/cm³,

length of the soil profile, CL = 100 cm,

$k_D = 0.1$ cm³/g,

$k_1 = 0.1$ hr⁻¹,

$k_2 = 0.0001$ hr⁻¹,

$k_3 = 0.001$ hr⁻¹,

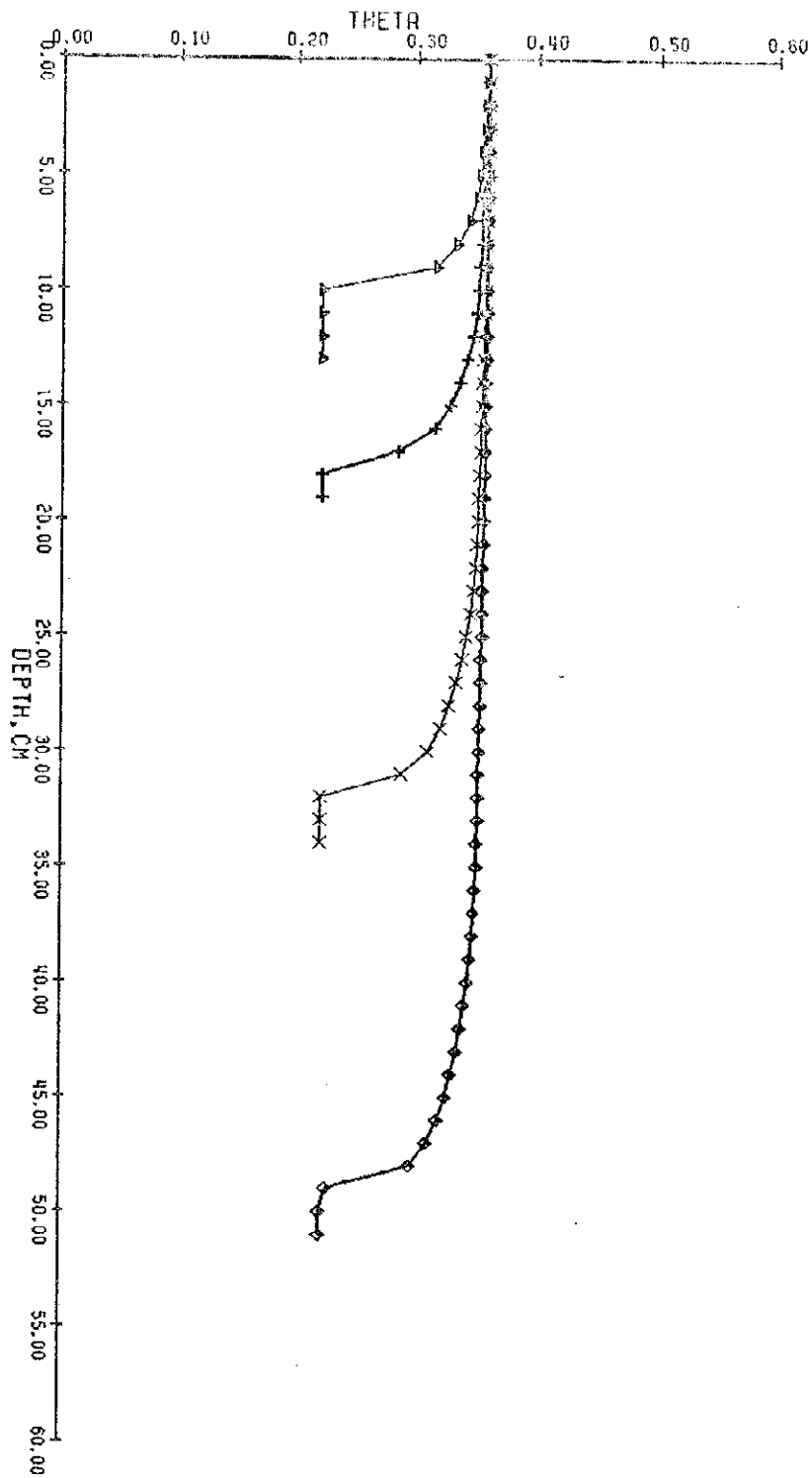
$k_4 = 0.001$ hr⁻¹,

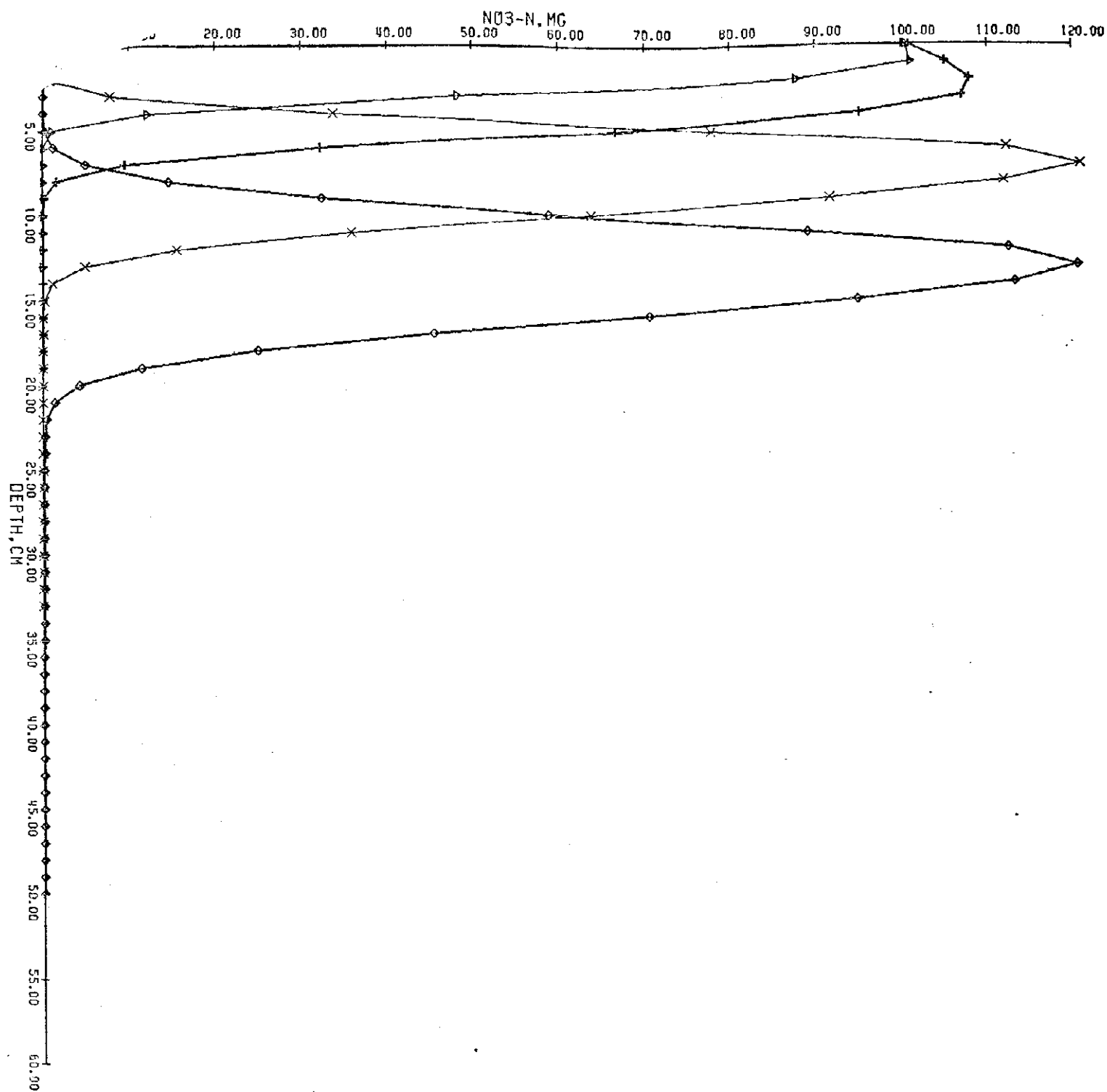
$k_5 = 0.0$ hr⁻¹.

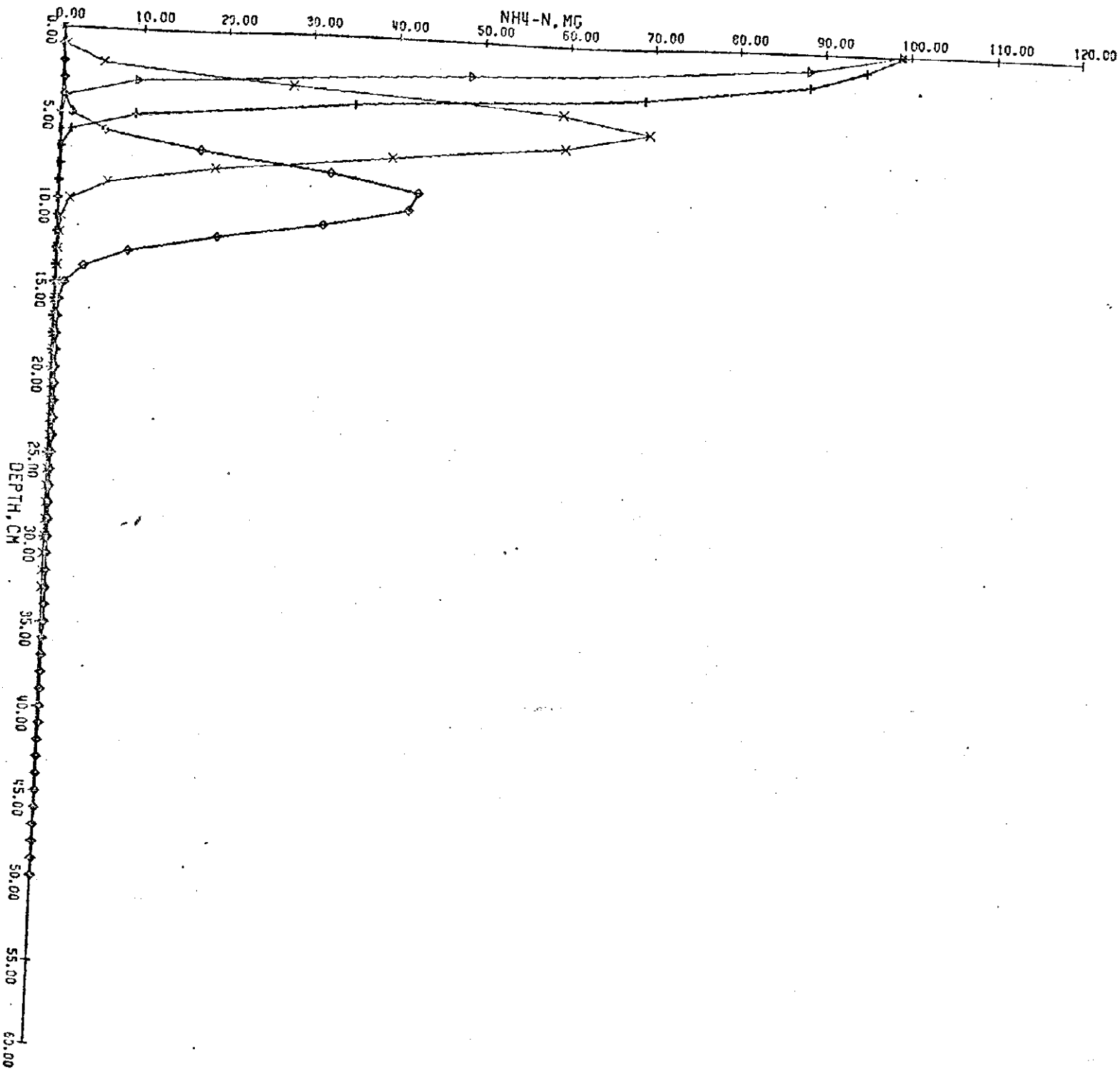
Finally, the dispersion coefficient D was considered as a function of the pore water velocity (q/ θ) as obtained by Kirda et al (1973),

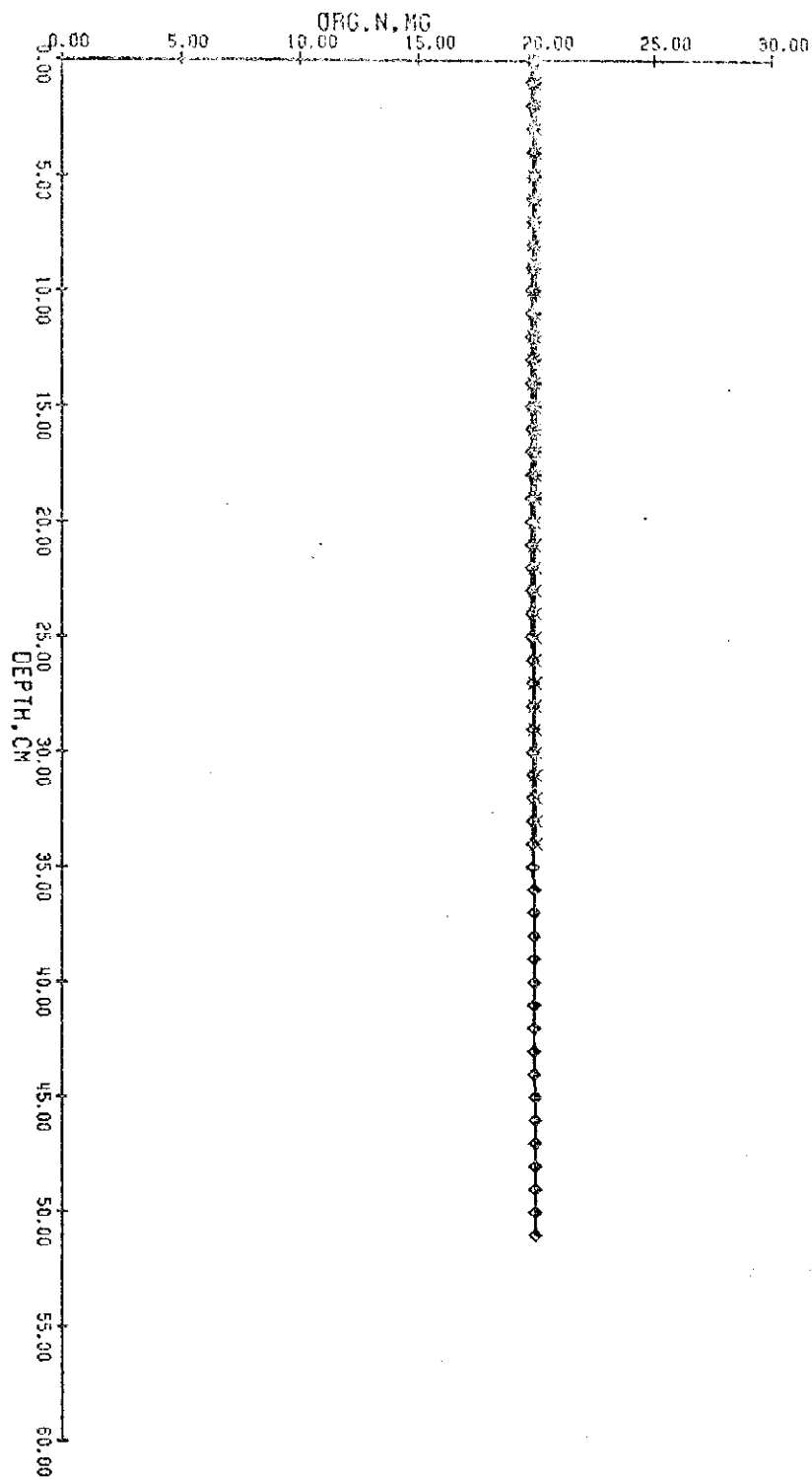
$$D = 0.0258 + 0.1274 (q/\theta)^{1.355} \quad \text{cm}^2/\text{hr}$$

Computer output results and GOULD plots are obtained for selected times of 1, 2, 5, and 10 hours. The total CPU time used in this program was 161.75 seconds.









94-SELIMA -FORT -SY3PRINT

FORTAN IV & LEVEL 21

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0001      COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
0002      *VP(810),DISPC(810)
0003      COMMON/L2/ AA(810),S2(810),CC(810),R(810),X(810)
0004      COMMON/L3/ N,NM1,NM2,NP1,NP2
0005      COMMON/L4/ ALPHA,BETA,DT,DZ
0006      COMMON/L5/ RKD,RK1,RK2,RK3,RK4,RK5
0007      COMMON/L6/ SFLUX,CSNH4,CSNO3
0008      COMMON/L7/ R0U,COLUMN,DFLUX
0009      COMMON/L8/ DISP,THMAX,THMIN,HMIN,CORGNI
0010      COMMON/L9/ TIME,TPRINT,TWRITE
0011      COMMON/L10/ H(810),CDN(810),CAP(810)
0012      COMMON/L11/ THC(30),HC(30),CAPC(30)
0013      COMMON/L12/ AC,BC,NX,NX1,CONST
0014      COMMON/L13/ WFLUX(810)
0015      COMMON/L14/ VD,TWC,TSALT
0016      COMMON/L15/ TIT(30),TC,DTDT,IT,IL,NT
0017      COMMON/L16/ IC,IWT
0018      COMMON/L17/ XXX(30),C1(30),C2(30),C3(30),C4(30),C5(30),C6(30)
0019      100 FORMAT(8F10.4)
0020      200 FORMAT(3E10.4)
0021      300 FORMAT(2I4)
0022      READ(5,300) NX
0023      NX1=NX-1
0024      READ(5,100) (THC(I),I=1,NX)
0025      WRITE(6,100) (THC(I),I=1,NX)
0026      READ(5,100) (HC(I),I=1,NX)
0027      WRITE(6,100) (HC(I),I=1,NX)
0028      READ(5,100) DZ,DT
0029      WRITE(6,100) DZ,DT
0030      READ(5,100) DISP,THMAX,THMIN,HMIN,CORGNI
0031      WRITE(6,100) DISP,THMAX,THMIN,HMIN,CORGNI
0032      READ(5,100) COLUMN,R0U,CSNH4,CSNO3,DFLUX
0033      WRITE(6,200) AC,BC,CONST
0034      READ(5,200) AC,BC,CONST
0035      WRITE(6,300) NT
0036      READ(5,100) (TIT(I),I=1,NT)
0037      WRITE(6,100) (TIT(I),I=1,NT)
0038      READ(5,100) RKD,RK1,RK2,RK3,RK4,RK5
0039      WRITE(6,100) RKD,RK1,RK2,RK3,RK4,RK5
0040      READ(5,300) NIT
0041      READ(5,100) (XXX(I),I=1,NIT)
0042      WRITE(6,100) (XXX(I),I=1,NIT)
0043      READ(5,100) (C1(I),I=1,NIT)
0044      WRITE(6,100) (C1(I),I=1,NIT)
0045      READ(5,100) (C2(I),I=1,NIT)
0046      WRITE(6,100) (C2(I),I=1,NIT)
0047      READ(5,100) (C3(I),I=1,NIT)
0048      WRITE(6,100) (C3(I),I=1,NIT)
0049      READ(5,100) (C4(I),I=1,NIT)
0050      WRITE(6,100) (C4(I),I=1,NIT)
0051      READ(5,100) (C5(I),I=1,NIT)
0052      WRITE(6,100) (C5(I),I=1,NIT)
0053      READ(5,100) (C6(I),I=1,NIT)
0054      WRITE(6,100) (C6(I),I=1,NIT)
0055      IT=1
0056      TC=TIT(IT)
0057      N=25
0058      NM1=N-1
0059      NM2=N-2
0060      NP1=N+1
0061      NP2=N+2
0062      TSALT=2.0
0063      TWC=10.0
0064      SFLUX=CONST
C
0065      CALL INITWT
0066      CALL INITST
0067      IC=2
0068      IWT=1
0069      CALL AXISPL
C
0070      H(1)=-100.0
0071      TIME=0.0
0072      CALL S3CW

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0073      99 CONTINUE
0074      IL=20
0075      DO 5 II=1,IL
0076      CALL WATER
0077      CALL AMONIA
0078      CALL NITRAT
0079      CALL GASORG
0080      5 CONTINUE
0081      TIME=TIME+IL*DT
0082      CALL DADJ
0083      TWRITE=ABS(TIME-TC)
0084      IF(TWRITE.LE.1.0E-3) CALL GRAPH
0085      IF(TIME.GE.TIT(NT)) CALL PLOT(0.0,0.0,999)
0086      IF(TWRITE.LE.1.0E-3) CALL OUTPUT
0087      IF(TIME.GE.TIT(NT)) STOP
0088      CALL CHECKT
0089      CALL CHECKN
0090      GO TO 99
0091      END
```

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```

0001      C
0002      SUBROUTINE MOISD(I1,I2)
0003      COMMON/L1/ TH(810),CNH4(810),CNU3(810),CURGN(810),CNU2(810),
0004      *VP(810),DISPC(810)
0005      COMMON/L3/ N,NM1,NM2,NF1,NP2
0006      COMMON/L4/ ALPHA,BETA,DT,DZ
0007      COMMON/L10/ H(810),CON(810),CAP(810)
0008      COMMON/L17/ XXX(30),C1(30),C2(30),C3(30),C4(30),C5(30),C6(30)
0009      I=1
0010      DO 20 K=I1,I2
0011      A=DZ*(K-1)
0012      5 IF(A.LE.XXX(I+1)) GO TO 10
0013      I=I+1
0014      GO TO 5
0015      10 H(K)=C1(I)+(A-XXX(I))*((C1(I+1)-C1(I))/(XXX(I+1)-XXX(I)))
0016      TH(K)=C2(I)+(A-XXX(I))*((C2(I+1)-C2(I))/(XXX(I+1)-XXX(I)))
0017      CNH4(K)=C3(I)+(A-XXX(I))*((C3(I+1)-C3(I))/(XXX(I+1)-XXX(I)))
0018      CNU3(K)=C4(I)+(A-XXX(I))*((C4(I+1)-C4(I))/(XXX(I+1)-XXX(I)))
0019      CURGN(K)=C5(I)+(A-XXX(I))*((C5(I+1)-C5(I))/(XXX(I+1)-XXX(I)))
0020      CNU2(K)=C6(I)+(A-XXX(I))*((C6(I+1)-C6(I))/(XXX(I+1)-XXX(I)))
0021      20 CONTINUE
0022      RETURN
0023      END

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0001      C      SUBROUTINE AXISPL
0002      COMMON/L16/IC,IWT
0003      XL=15.0
0004      YL=7.0
0005      XSIZE=12.01
0006      YSIZE1=6.010
0007      YSIZE2=12.010
0008      CALL PLOTS(-40.0,-20.0)
0009      CALL PLOT(1.0,1.0,-3)
0010      CALL LINEWT(IWT)
0011      CALL AXIS(0.0,0.0,'DEPTH,CM',-8.XSIZE,0.0,0.0,5.00)
0012      CALL AXIS(0.0,0.0,' THETA ',8.YSIZE1,90.0,0.0,10.0)
0013      CALL PLOT(0.0,YL,-3)
0014      CALL AXIS(0.0,0.0,'DEPTH,CM',-8.XSIZE,0.0,0.0,5.00)
0015      CALL AXIS(0.0,0.0,'NH4-N,MG',8.YSIZE2,90.0,0.0,10.0)
0016      CALL PLOT(XL,-YL,-3)
0017      CALL AXIS(0.0,0.0,'DEPTH,CM',-8.XSIZE,0.0,0.0,5.00)
0018      CALL AXIS(0.0,0.0,'ORG-N,MG',8.YSIZE1,90.0,0.0,5.00)
0019      CALL PLOT(0.0,YL,-3)
0020      CALL AXIS(0.0,0.0,'DEPTH,CM',-8.XSIZE,0.0,0.0,5.00)
0021      CALL AXIS(0.0,0.0,'NO3-N,MG',8.YSIZE2,90.0,0.0,10.0)
0022      CALL PLOT(-XL,-YL,-3)
0023      RETURN
0024      END

```

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0001      C
0002      SUBROUTINE GRAPH
0003      COMMON/L1/ TH(810),CNH4(810),CND3(810),CORGN(810),CND2(810),
0004      *VP(810),DISPC(810)
0005      COMMON/L3/ N,N41,NM2,NP1,NP2
0006      COMMON/L4/ ALPHA,BETA,DF,DZ
0007      COMMON/L16/IC,IWT
0008      CALL LINEWT(IWT)
0009      XL=15.0
0010      YL=7.0
0011      KK=1.0/DZ+0.010
0012      KKK=N
0013      IF((DZ*N).GT.120.0) KKK=120*KK-1
0014      SYMSZ=0.100
0015      C
0016      X1=0.0
0017      DO 10 I=1,KKK,KK
0018      YS=TH(I)*10.0
0019      XS=X1/5.0
0020      CALL SYMBOL(XS,YS,SYMSZ,IC,0.0,-2)
0021      X1=X1+1.0
0022      10 CONTINUE
0023      CALL PLOT(0.0,YL,-3)
0024      X1=0.0
0025      DO 20 I=1,KKK,KK
0026      YS=CNH4(I)/10.0
0027      XS=X1/5.0
0028      CALL SYMBOL(XS,YS,SYMSZ,IC,0.0,-2)
0029      X1=X1+1.0
0030      20 CONTINUE
0031      CALL PLOT(XL,-YL,-3)
0032      X1=0.0
0033      DO 30 I=1,KKK,KK
0034      YS=CORGN(I)/5.0
0035      XS=X1/5.0
0036      CALL SYMBOL(XS,YS,SYMSZ,IC,0.0,-2)
0037      X1=X1+1.0
0038      30 CONTINUE
0039      CALL PLOT(0.0,YL,-3)
0040      X1=0.0
0041      DO 40 I=1,KKK,KK
0042      YS=CND3(I)/10.0
0043      XS=X1/5.0
0044      CALL SYMBOL(XS,YS,SYMSZ,IC,0.0,-2)
0045      X1=X1+1.0
0046      40 CONTINUE
0047      CALL PLOT(-XL,-YL,-3)
0048      IC=IC+1
0049      IF(IC.GT.7) IC=0
0050      IWT=IWT+1
0051      IF(IWT) 1,2,2
0052      2 IWT=-2
0053      RETURN
0054      1 IWT=-1
0055      RETURN
0056      END

```

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```
      C
0001      SUBROUTINE CHECKT
0002      COMMON/L4/ ALPHA,BETA,DT,DZ
0003      COMMON/L9/TIME,TPRINT,TWRITE
0004      COMMON/L15/ TIT(30),TC,DTOT,IT,IL,NT
0005      DTOT=DT
0006      TWRITE=ABS(TIME-TC)
0007      IF(TWRITE.LT.1.0E-3) RETURN
0008      TIME10=TIME+IL*DT
0009      IF((TIME.LT.TC).AND.(TIME10.GE.TC)) GO TO 30
0010      RETURN
0011 30 DT=(TC-TIME)/IL
0012      ALPHA=DT/(2.0*DZ*DZ)
0013      BETA=DT/DZ
0014      RETURN
0015      END
```

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C *****
0011 SUBROUTINE XATE1
0012 CCOMMON/L1/ TH(610),CON(610),CON2(610),CORGN(610),CON2(610),
*VP(610),DISPC(610)
0013 CCOMMON/L2/ AA(610),BB(610),CC(610),R(610),X(610)
0014 CCOMMON/L3/ N,NM1,NM2,NP1,NP2
0015 CCOMMON/L4/ ALPHA,BETA,DT,DZ
0016 CCOMMON/L5/ PK0,PK1,PK2,PK3,PK4,PK5
0017 CCOMMON/L6/ SFLUX,CONH4,CONC3
0018 CCOMMON/L7/ BOO
0019 CCOMMON/L8/ DISP,THMAX,THMIN,HMIN,CORGN1
0020 CCOMMON/L9/ TIME,TPOINT,TWRITE
0021 CCOMMON/L10/ H(610),CON(610),CAP(610)
0022 CCOMMON/L11/ THC(30),HC(30),CAPC(30)
0023 CCOMMON/L12/ AC,BC,NX,NX1,CONST
0024 CCOMMON/L13/ WFLUX(610)
0025 CCOMMON/L14/ VC,TWD,TSALT
0026 DO 20 I=1,NP1
0027 90 CON(I)=AC*EXP(PC*(TH(I)+TH(I+1))*0.50)
C
0028 DO 1 I=1,NM2
0029 AA(I)=CAP(I+1)+ALPHA*(CON(I+1)+CON(I))
0030 BB(I)=-ALPHA*CON(I+1)
0031 CC(I)=-ALPHA*CON(I+1)
0032 1 CONTINUE
0033 AA(NM1)=CAP(N)+ALPHA*CON(N)
0034 DO 2 I=1,NM1
0035 X1=CAP(I+1)*H(I+1)
0036 X2=ALPHA*CON(I)*H(I)-ALPHA*H(I+1)*(CON(I+1)+CON(I))
0037 X3=ALPHA*CON(I+1)*H(I+2)
0038 X4=-BETA*(CON(I+1)-CON(I))
0039 R(I)=X1+X2+X3+X4
0040 2 CONTINUE
0041 R(1)=R(1)+ALPHA*CON(1)*H(1)
0042 CALL THIRM(AA,BB,CC,R,X,NM1)
0043 DO 3 K=2,N
0044 H(K)=X(K-1)
0045 H(NP1)=H(N)
0046 H(NP2)=H(N)
0047 CALL SRCW
0048 DO 15 J=1,NP2
0049 IF(H(J).LT.HC(1)) GO TO 25
0050 TH(J)=TH(1)
0051 15 CAP(J)=CAP(1)
0052 25 CONTINUE
0053 DO 60 I=J,NP2
0054 DO 80 K=1,NX1
0055 IF(H(I).GT.HC(K+1)) GO TO 70
0056 80 CONTINUE
0057 70 TH(I)=THC(K)+CAPC(K)*(H(I)-HC(K))
0058 CAP(I)=CAPC(K)
0059 60 CONTINUE
0060 DO 95 I=1,NP1
0061 WFLUX(I)=-CON(I)*(H(I+1)-H(I))/DZ+CON(I)
0062 DISPC(I)=0.02580+0.12740*ABS(WFLUX(I)/TH(I))*1.3550
0063 95 CONTINUE
0064 RETURN
0065 END

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C
C
0001 SUBROUTINE INITWT
0002 COMMON/L1/ H(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
C VP(810),DTSPC(810)
0003 COMMON/L2/ AA(610),BB(610),CC(610),R(610),X(610)
0004 COMMON/L3/ N,NM1,NM2,NP1,NP2
0005 COMMON/L4/ ALPHA,BETA,DT,DZ
0006 COMMON/L5/ RKD,RK1,RK2,RK3,RK4,RK5
0007 COMMON/L6/ SFLUX,CSNH4,CNO3
0008 COMMON/L7/ RDU
0009 COMMON/L8/ DTSP,THMAX,THMIN,HMIN,CORGN1
0010 COMMON/L9/ TIME,TPRINT,TWRITE
0011 COMMON/L10/ H(810),CON(810),CAP(810)
0012 COMMON/L11/ THC(30),HC(30),CAPC(30)
0013 COMMON/L12/ AC,BC,NX,NX1,CONST
0014 COMMON/L13/ SFLUX(810)
0015 COMMON/L14/ V0,TWO,TSALT
0016 COMMON/L17/ XXX(30),C1(30),C2(30),C3(30),C4(30),C5(30),C6(30)
0017 DO 5 I=1,NX1
0018 CAPC(I)=(THC(I+1)-THC(I))/(HC(I+1)-HC(I))
0019 5 CONTINUE
0020 CAPC(NX)=CAPC(NX1)
C
C
0021 5 CONTINUE
0022 ALPHA=DT/(2.0+DZ*DZ)
0023 BETA=DT/DZ
0024 TTT=CONST/CAPC(1)
0025 TTT=TTT*ALPHA
0026 IF(TTT.LE.2.00) GO TO 8
0027 IF(DZ.GE.0.999) GO TO 7
0028 DZ=DZ*2.0
0029 GO TO 5
0030 7 DT=DT/2.0
0031 GO TO 5
0032 8 CONTINUE
0033 CALL M0150(1,NP2)
0034 CALL SBC#
0035 DO 25 I=1,NP2
0036 DO 15 K=1,NX1
0037 IF(H(I).GT.HC(K+1)) GO TO 20
0038 15 CONTINUE
0039 20 CAP(I)=CAPC(K)
0040 25 CONTINUE
0041 RETURN
0042 END

```

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C
C
C *****
0001 SUBROUTINE SBCW
0002 COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
      *VP(510),DISPC(910)
0003 COMMON/L2/ AA(610),JB(610),CC(610),R(510),X(610)
0004 COMMON/L3/ N,NM1,NM2,NP1,NP2
0005 COMMON/L4/ ALPHA,BETA,DT,DZ
0006 COMMON/L5/ PKO,PK1,PK2,PK3,PK4,PK5
0007 COMMON/L6/ SFLUX,CSNH4,CSNO3
0008 COMMON/L7/ ROU
0009 COMMON/L8/ DISP,THMAX,THMIN
0010 COMMON/L9/ TIME,TPRINT,TWRITE
0011 COMMON/L10/ H(810),CON(810),CAP(810)
0012 COMMON/L11/ TH(130),HC(130),CAPC(130)
0013 COMMON/L12/ AC,CC,NX,NX1,CONST
0014 COMMON/L13/ WFLUX(810)
0015 COMMON/L14/ VO,TWO,TSALT
0016 IF(SFLUX.GT.0.0) GO TO 5
0017 CONS=AC*EXP(BC*TH(1))
0018 ADJ=DZ*(1.0-SFLUX/CONS)
0019 H(1)=H(2)-ADJ
0020 IF(H(1).LT.(-1900.0)) H(1)=-1900.0
0021 RETURN
C
C 5 CONTINUE
0022 H(1)=H(1)+0.400
0023 IF(H(1).GT.0.0) H(1)=0.0
0024 RETURN
0025 END
0026

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C
C
C *****
0001 SUBROUTINE INITST
0002 COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
      *VP(810),DISPC(810)
0003 COMMON/L2/ AA(810),RE(810),CC(810),R(810),X(810)
0004 COMMON/L3/ N,NM1,NM2,NP1,NP2
0005 COMMON/L4/ ALPHA,BETA,DT,DZ
0006 COMMON/L5/ RK0,RK1,RK2,RK3,RK4,RK5
0007 COMMON/L6/ SFLUX,CSNH4,CSNO3
0008 COMMON/L7/ ROU
0009 COMMON/L8/ DISP,THMAX,THMIN,HMIN,CORGNI
0010 COMMON/L9/ TIME,TPRINT,TWRITE
0011 COMMON/L10/ H(810),CON(810),CAP(810)
0012 COMMON/L11/ THC(30),HC(30),CAPC(30)
0013 COMMON/L12/ AC,BC,NX,NX1,CONST
0014 COMMON/L13/ SFLUX(810)
0015 COMMON/L14/ VO,TAD,TSALT
0016 COMMON/L17/ XXX(30),C1(30),C2(30),C3(30),C4(30),C5(30),C6(30)
C
0017 THAVR=(THMAX+THMIN)/2
0018
0019 1 CONTINUE
0020 APAR=SFLUX-DISP*(TH4IN-THAVR)/DZ
0021 APAR=SFLUX-DISP*(THMIN-THMAX)/DZ
0022 VC=APAR/THAVR
0023 VD=SFLUX/THMAX
0024 V0=APAR/THMIN
0025 ALPHA=DT/(2.0*DZ*DZ)
0026 BETA=DT/DZ
0027 DVC=DISP/V0
0028 DZV0=2.50*DZ/V0
0029 IF(DZ*.51.DVC) GO TO 2
0030 IF(DT*.51.DZV0) GO TO 3
0031 GO TO 4
0032 2 DZ=DZ/2
0033 GO TO 1
0034 3 DT=DT/2
0035 GO TO 1
0036 4 CONTINUE
0037 6 CONTINUE
0038 ALPHA=DT/(2.0*DZ*DZ)
0039 BETA=DT/DZ
0040 TTT=CONST/CAPC(1)
0041 TTT=TTT*ALPHA
0042 IF(TTT,LE,2.00) GO TO 8
0043 DT=DT/2.0
0044 GO TO 6
0045 8 CONTINUE
0046 CALL MOISD(1,NP2)
0047 RETURN
      END

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C
C
C *****
0001 SUBROUTINE DADJ
0002 COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGNI(810),CNO2(810),
      *VP(810),DISPC(810)
0003 COMMON/L2/ AA(610),BB(610),CC(610),R(610),X(610)
0004 COMMON/L3/ N,NM1,NM2,NP1,NP2
0005 COMMON/L4/ ALPHA,BETA,DT,DZ
0006 COMMON/L5/ RK0,RK1,RK2,RK3,RK4,RK5
0007 COMMON/L6/ SFLUX,CSNH4,CSNO3
0008 COMMON/L7/ROU,COLUMN,DFLUX
0009 COMMON/L8/ DISP,THMAX,THMIN,HMIN,CGRNI
0010 COMMON/L9/TIME,TPRINT,TWRITE
0011 COMMON/L10/ H(810),CEN(810),CAP(810)
0012 COMMON/L11/ THC(30),PC(30),CAPC(30)
0013 COMMON/L12/ AC,BC,NX,NX1,CONST
0014 COMMON/L13/ *FLUX(810)
0015 COMMON/L14/ V0,TWD,TSALT
0016 COMMON/L17/ XXX(30),C1(30),C2(30),C3(30),C4(30),C5(30),C6(30)
0017 IF(A35(TIME-TWDT),GT,1.0E-3) GO TO 5
0018 CSNH4=0.0
0019 CSNO3=0.0
0020 5 CONTINUE
0021 IF(A35(TIME-TWD),GT,1.0E-3) GO TO 10
0022 SFLUX=DFLUX
0023 10 CONTINUE
0024 IF(TIME,GT,TWD) CALL DADJO
0025 KK=2
0026 IF((KK*ALPHA),GT,0.20) RETURN
0027 L=10
0028 V1=VP(L)/TH(L)
0029 IF(V1,LT,0.050) V1=0.050
0030 DZV0=C,50*DZ/V1
0031 IF((DT*KK),LT,0.0ZV0) DT=DT*KK
0032 ALPHA=DT/(2.0*DZ*DZ)
0033 BETA=DT/DZ
0034 IF(A35(TH(L)-THMIN),LT,0.0550) RETURN
0035 DVO=0.50*DISPC(L)/V1
0036 IF((DZ*KK),GT,DVO) RETURN
0037 DZ=DZ*KK
0038 M=1
0039 DO 15 I=1,NP1,KK
0040 H(M)=H(I)
0041 TH(M)=TH(I)
0042 CAP(M)=CAP(I)
0043 CNO2(M)=CNO2(I)
0044 CNH4(M)=CNH4(I)
0045 CORGNI(M)=CORGNI(I)
0046 DISPC(M)=DISPC(I)
0047 M=M+1
0048 15 CONTINUE
0049 CALL MOISD(M,NP2)
0050 DO 35 J=M,NP2
0051 DO 25 K=1,NX1
0052 IF(H(I),GT,HC(K+1)) GO TO 30
0053 25 CONTINUE
0054 30 CAP(I)=CAPC(K)
0055 35 CONTINUE
0056 ALPHA=DZ/(2.0*DZ*DZ)
0057 BETA=DT/DZ
0058 RETURN
0059 END

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C
0001      SUBROUTINE DADJD
0002      COMMON/L1/ TH(810),CNH4(610),CNO3(810),CORGN(810),CNO2(810),
      *VP(310),DISPC(810)
0003      COMMON/L2/ AA(610),BE(610),CC(610),K(610),X(610)
0004      COMMON/L3/ N,NM1,NM2,NP1,NP2
0005      COMMON/L4/ ALPHA,BETA,DT,DZ
0006      COMMON/L5/ RKD,RK1,RK2,RK3,RK4,RK5
0007      COMMON/L6/ SFLUX,CSNH4,CSNO3
0008      COMMON/L7/ RDU
0009      COMMON/L8/ DISP,THMAX,THMIN,HMIN,CORGNI
0010      COMMON/L9/ TIME,TPRINT,TWRITE
0011      COMMON/L10/ H(810),CON(810),CAP(810)
0012      COMMON/L11/ THC(30),HC(30),CAPC(30)
0013      COMMON/L12/ AC,SC,NX,NX1,CONST
0014      COMMON/L13/ WFLUX(810)
0015      COMMON/L14/ VO,T40,TSALT
0016      COMMON/L17/ XXX(30),C1(30),C2(30),C3(30),C4(30),C5(30),C6(30)
0017      DTT=DT
0018      DZZ=DZ
0019      KK=2
0020      L=10
0021      VI=VP(L)/TH(L)
0022      IF(VI.LT.0.0250) VI=0.0250
0023      DV0=0.50*DZ/VI
0024      IF((DT*KK).LT.DV0) DTT=DT*KK
0025      DV0=0.50*DISPC(L)/VI
0026      IF((DZ*KK).GT.DV0) KK=1
0027      DZZ=DZ*KK
0028      ALPHAN=DTT/(2.0*DZZ*DZZ)
0029      IF(ALPHAN.GT.0.20) RETURN
0030      DT=DTT
0031      DZ=DZZ
0032      ALPHA=DT/(2.0*DZ*DZ)
0033      BETA=DT/DZ
0034      IF(KK.GT.1) GO TO 5
0035      RETURN
0036      5 CONTINUE
0037      M=1
0038      DO 15 I=1,NP1,KK
0039      H(M)=H(I)
0040      TH(M)=TH(I)
0041      CAP(M)=CAP(I)
0042      CNO3(M)=CNO3(I)
0043      CNH4(M)=CNH4(I)
0044      CORGN(M)=CORGN(I)
0045      DISPC(M)=DISPC(I)
0046      M=M+1
0047      15 CONTINUE
0048      CALL MOISD(M,NP2)
0049      DO 35 I=M,NP2
0050      DO 25 K=1,NX1
0051      IF(H(I).GT.HC(K+1)) GO TO 30
0052      25 CONTINUE
0053      CAP(I)=CAPC(K)
0054      35 CONTINUE
0055      RETURN
0056      END

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C
0001 SUBROUTINE CHECKN
0002 COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
*VP(810),DISPC(810)
0003 COMMON/L1/ N,NM1,NM2,NP1,NP2
0004 COMMON/L4/ ALPHA,BETA,DT,OZ
0005 COMMON/L5/ RKD,RK1,RK2,RK3,RK4,RK5
0006 COMMON/L6/ SFLUX,CSNH4,CSNJ3
0007 COMMON/L7/RCU,COLUMN,DFLUX
0008 COMMON/L8/ DISP,THMAX,THMIN,HMIN,CORGNI
0009 COMMON/L9/TIME,TPRINT,TWRITE
0010 COMMON/L10/ H(810),CON(810),CAP(810)
0011 COMMON/L11/ THC(30),HC(30),CAPC(30)
0012 COMMON/L12/ AG,SC,NA,NX1,CONST
0013 COMMON/L13/ WFLUX(810)
0014 COMMON/L14/ VO,TWD,TSALT
0015 COMMON/L15/ TIT(30),TC,DTDT,IT,IL,NT
0016 COMMON/L17/ XXX(30),C1(30),C2(30),C3(30),C4(30),C5(30),C6(30)
0017 NM=10
0018 NMIF=COLUMN/DZ
0019 IF(N-NMIF) 10,3,20
0020 5 RETURN
0021 10 IF(N.GT.500) RETURN
0022 IF(ABS(TH(N-20)-THMIN).LT.0.0020) RETURN
0023 NMIF=NM
0024 NNNN=NMIF+2
0025 CALL MD15D(NP1,NNNN)
0026 DO 15 I=NP1,NNNN
0027 DO 17 K=1,NX
0028 IF(H(I).GT.HC(K+1)) GO TO 18
0029 17 CONTINUE
0030 15 CAP(I)=CAPC(K)
0031 16 CONTINUE
0032 20 N=NMIF
0033 NM1=N-1
0034 NM2=N-2
0035 NP1=N+1
0036 NP2=N+2
0037 RETURN
0038 END

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C
C
C *****
0001      SUBROUTINE AMONIA
0002      NH=4      PROGRAM
C      COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
      *VP(810),DISPC(810)
0003      COMMON/L2/ AA(510),BB(610),CC(610),R(610),X(610)
0004      COMMON/L3/ N,NM1,NM2,NP1,NP2
0005      COMMON/L4/ ALPHA,BETA,DT,DZ
0006      COMMON/L5/ RKD,RK1,RK2,RK3,RK4,RK5
0007      COMMON/L6/ SFLUX,CSNH4,CSNJ3
0008      COMMON/L7/ ROU
0009      COMMON/L8/ DISP,THMAX,THMIN,HMIN,CORGN1
0010      COMMON/L9/ TIME,TPRINT,TWRITE
0011      COMMON/L10/ H(810),CON(810),CAP(810)
0012      COMMON/L11/ THC(30),HC(30),CAPC(30)
0013      COMMON/L12/ AC,BC,NX,NX1,CONST
0014      COMMON/L13/ WFLUX(810)
0015      COMMON/L14/ VO,TWO,TSALT
0016      FF=2.0*DZ
0017      SSINF=WFLUX(1)
0018      CNH4(1)=(SSINF*FF*CSNH4+DISP*TH(1)*CNH4(3))/(SSINF*FF+DISP*TH(1))
0019      DO 11 I=1,NP1
0020      DISP=DISPC(I)
0021      VP(1)=WFLUX(1)-DISP*(TH(1+1)-TH(1))/DZ
0022      1 CONTINUE
0023      IF(SFLUX.LE.0.0) GO TO 13
0024      DO 5 I=1,NM2
0025      DISP=DISPC(I+1)
0026      RKK=1.0+RKO*ROU/TH(I+1)
0027      AA(I)=RKK+2.0*ALPHA*DISP-BETA*VP(I+1)/TH(I+1)
0028      BB(I)=BETA*VP(I+1)/TH(I+1)-ALPHA*DISP
0029      DISP=DISPC(I+2)
0030      CC(I)=ALPHA*DISP
0031      5 CONTINUE
0032      DISP=DISPC(N)
0033      RKK=1.0+RKO*ROU/TH(N)
0034      AA(NM1)=RKK+ALPHA*DISP
0035      DO 10 M=1,NM1
0036      I=M+1
0037      DISP=DISPC(I)
0038      RKK=1.0+RKO*ROU/TH(I)
0039      R(M)=RKK*CNH4(I)+ALPHA*DISP*(CNH4(I+1)-2.0*CNH4(I)+CNH4(I-1))
0040      R(M)=R(M)-DT*(RKK+RKK4)*CNH4(I)+(ROU*DT/TH(I))*RK3*CORGN(I)
0041      10 CONTINUE
0042      DISP=DISPC(2)
0043      R(1)=R(1)+ALPHA*DISP*CNH4(1)
0044      GO TO 14
C
0045      13 CONTINUE
0046      CNH4(1)=CNH4(2)
0047      DO 11 I=1,NM2
0048      DISP=DISPC(I+1)
0049      RKK=1.0+RKO*ROU/TH(I+1)
0050      AA(I)=RKK+2.0*ALPHA*DISP-BETA*VP(I+1)/TH(I+1)
0051      BB(I)=BETA*VP(I+1)/TH(I+1)-ALPHA*DISP
0052      DISP=DISPC(I+2)
0053      CC(I)=ALPHA*DISP
0054      11 CONTINUE
0055      DISP=DISPC(N)
0056      RKK=1.0+RKO*ROU/TH(N)
0057      AA(NM1)=RKK+ALPHA*DISP
0058      DISP=DISPC(2)
0059      RKK=1.0+RKO*ROU/TH(2)
0060      AA(1)=RKK+1.0*ALPHA*DISP-BETA*VP(2)/TH(2)
0061      DO 12 M=1,NM1
0062      I=M+1
0063      DISP=DISPC(I)
0064      RKK=1.0+RKO*ROU/TH(I)
0065      R(M)=RKK*CNH4(I)+ALPHA*DISP*(CNH4(I+1)-2.0*CNH4(I)+CNH4(I-1))
0066      R(M)=R(M)-DT*(RKK+RKK4)*CNH4(I)+(ROU*DT/TH(I))*RK3*CORGN(I)
0067      12 CONTINUE
0068      14 CONTINUE
0069      CALL TRIDM(AA,BB,CC,R,X,NM1)
0070      DO 15 I=2,N
0071      CNH4(I)=X(I-1)
0072      CNH4(NP1)=CNH4(N)

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0073
0074

RETURN
END

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C
C
C *****
0001 SUBROUTINE NITRAT
0002 NO-3 PROGRAM
COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
*VP(810),DISPC(810)
0003 COMMON/L2/ AA(810),BB(810),CC(810),R(810),X(810)
0004 COMMON/L3/ N,NM1,NM2,NP1,NP2
0005 COMMON/L4/ ALPHA,BETA,DT,DZ
0006 COMMON/L5/ RKD,RK1,RK2,RK3,RK4,RK5
0007 COMMON/L6/ SFLUX,CSNH4,CSNO3
0008 COMMON/L7/ ROU
0009 COMMON/L8/ DISP,THMAX,THMIN,HMIN,CORGNI
0010 COMMON/L9/ TIME,TPRINT,TWRITE
0011 COMMON/L10/ H(810),CON(810),CAP(810)
0012 COMMON/L11/ THC(30),HC(30),CAPC(30)
0013 COMMON/L12/ AC,BC,NX,NX1,CONST
0014 COMMON/L13/ WFLUX(810)
0015 COMMON/L14/ VO,TWD,TSALT
0016 FF=2.0*DZ
0017 SSINF=WFLUX(1)
0018 CNO3(1)=(SSINF*FF*CSNO3+DISP*TH(1)*CNO3(3))/(SSINF*FF+DISP*TH(1))
0019 IF(SFLUX.LE.0.0) GO TO 13
0020 DO 5 I=1,NM2
0021 DISP=DISPC(I+1)
0022 AA(I)=1.0+2.0*ALPHA*DISP-BETA*VP(I+1)/TH(I+1)
0023 BB(I)=BETA*VP(I+1)/TH(I+1)-ALPHA*DISP
0024 DISP=DISPC(I+2)
0025 CC(I)=-ALPHA*DISP
0026 5 CONTINUE
0027 DISP=DISPC(N)
0028 AA(NM1)=1.0+ALPHA*DISP
0029 DO 10 M=1,NM1
0030 I=M+1
0031 DISP=DISPC(I)
0032 R(M)=CNO3(I)+ALPHA*DISP*(CNO3(I+1)-2.0*CNO3(I)+CNO3(I-1))
0033 R(M)=R(M)+RK1*DT*CNH4(I)-DT*(RK2+RK5)*CNO3(I)
0034 10 CONTINUE
0035 DISP=DISPC(2)
0036 R(1)=R(1)+ALPHA*DISP*CNO3(1)
0037 GO TO 14
C
13 CONTINUE
CNO3(1)=CNO3(2)
DO 11 I=1,NM2
DISP=DISPC(I+1)
AA(I)=1.0+2.0*ALPHA*DISP-BETA*VP(I+1)/TH(I+1)
BB(I)=BETA*VP(I+1)/TH(I+1)-ALPHA*DISP
DISP=DISPC(I+2)
CC(I)=-ALPHA*DISP
11 CONTINUE
DISP=DISPC(N)
AA(NM1)=1.0+ALPHA*DISP
DISP=DISPC(2)
AA(1)=1.0+1.0*ALPHA*DISP-BETA*VP(2)/TH(2)
DO 12 M=1,NM1
I=M+1
DISP=DISPC(I)
R(M)=CNO3(I)+ALPHA*DISP*(CNO3(I+1)-2.0*CNO3(I)+CNO3(I-1))
R(M)=R(M)+RK1*DT*CNH4(I)-DT*(RK2+RK5)*CNO3(I)
12 CONTINUE
14 CONTINUE
CALL TRIDM(AA,BB,CC,R,X,NM1)
DO 15 I=2,N
CNO3(I)=X(I-1)
CNO3(NP1)=CNO3(N)
RETURN
END
0058
0059
0060
0061
0062
0063

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C *****
C
0001 SUBROUTINE GASORG
0002 COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
      *VP(810),DISPC(810)
0003 COMMON/L2/ AA(810),BB(810),CC(810),R(810),X(810)
0004 COMMON/L3/ N,NM1,NM2,NP1,NP2
0005 COMMON/L4/ ALPHA,BETA,DT,DZ
0006 COMMON/L5/ RK0,RK1,RK2,RK3,RK4,RK5
0007 COMMON/L6/ SFLUX,CSNH4,CSNJ3
0008 COMMON/L7/ EQU
0009 COMMON/L8/ DISP,THMAX,THMIN
0010 COMMON/L9/ TIME,TPRINT,TWRITE
0011 COMMON/L10/ H(810),CON(810),CAP(810)
0012 COMMON/L11/ #FLUX(810)
0013 COMMON/L14/ V0,TWO,TSALT
0014 DO 5 I=1,NP1
0015 CORGN(I)=CORGN(I)+(DT/ROU)*(TH(I)*RK2*CNO3(I)+TH(I)*RK4*CNH4(I)-
      *ROU*RK3*CORGN(I))
0016 5 CONTINUE
0017 DO 10 I=1,NP1
0018 CNO2(I)=CNO2(I)+(DT/ROU)*RK5*TH(I)*CNO3(I)
0019 10 CONTINUE
0020 RETURN
0021 END

```


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C
C
*****
0001 SUBROUTINE OUTPUT
0002 COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
0003 *VP(810),DISPC(810)
0004 COMMON/L2/ AA(810),JB(810),CC(810),RI(810),X(810)
0005 COMMON/L3/ N,NM1,NM2,NP1,NP2
0006 COMMON/L4/ ALPHA,BETA,DT,DZ
0007 COMMON/L5/ RKD,RK1,RK2,RK3,RK4,RK5
0008 COMMON/L6/ SFLUX,CSNH4,CSNJ3
0009 COMMON/L7/ RJU
0010 COMMON/L8/ DISP,THMAX,THMIN,HMIN,CORGN1
0011 COMMON/L9/ TIME,TPRINT,TWRITE
0012 COMMON/L10/ H(810),CON(810),CAP(810)
0013 COMMON/L11/ THC(30),HC(30),CAPC(30)
0014 COMMON/L12/ AC,BC,NX,NX1,CONST
0015 COMMON/L13/ *FLUX(810)
0016 COMMON/L14/ V0,TWD,TSALT
0017 COMMON/L15/ TIT(30),TC,CTDT,IT,IL,NT
0018
100
200 FORMAT(///,50X,'TIME = ',E12.5//,4X,'DEPTH,CM',4X,'SUCTION,CM',
0019 *4X,'THETA',7X,'HYDR.COND.',T56,'WATER FLUX',
0020 *T72,'NH4',T65,'NO3',T97,'CORGN',5X,' NO2')
0021
400 FORMAT(10E13.4)
0022 WRITE(6,100)
0023 TIME=TC
0024 WRITE(6,200) TIME
0025 DO 20 I=1,NP1
0026 ZZ=(1-I)*DZ
0027 WRITE(6,400) ZZ,H(I),TH(I),CON(I),*FLUX(I),CNH4(I),CNO3(I),
0028 *CORGN(I),CNO2(I)
0029
20 CONTINUE
0030 CALL TINT
0031 IT=IT+1
0032 IF(IT.GT.NT) STOP
0033 TC=TIT(IT)
0034 DT=CTDT
0035 ALPHA=DT/(2.0*DZ*DZ)
0036 BETA=DT/DZ
0037
25 CONTINUE
0038 KK=2
0039 TIT=CONST/CAPC(1)
0040 TIT=FIT*ALPHA
0041 IF(TIT.LE.2.00) GO TO 30
0042 RETURN
0043
30 CONTINUE
0044 DZV0=0.50*DZ/(VP(10)/TH(10))
0045 IF((DT*KK).LT.DZV0) DT=DT*KK
0046 ALPHA=DT/(2.0*DZ*DZ)
0047 BETA=DT/DZ
0048 RETURN
0049 END

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C
C *****
0001 SUBROUTINE TINT
0002 COMMON/L1/ TH(810),CNH4(810),CNO3(810),CORGN(810),CNO2(810),
*VP(810),DISPC(810)
0003 COMMON/L2/ AA(610),BB(610),CC(610),R(610),X(610)
0004 COMMON/L3/ N,NM1,NM2,NP1,NP2
0005 COMMON/L4/ ALPHA,BETA,OT,DZ
0006 COMMON/L5/ RKD,RK1,RK2,RK3,RK4,RK5
0007 COMMON/L6/ SFLUX,CSNH4,CSNJ3
0008 COMMON/L7/ ROU
0009 COMMON/L8/ DISP,THMAX,THMIN
0010 COMMON/L9/ TIME,TPRINT,TWRITE
0011 COMMON/L10/ H(810),CCN(810),CAP(810)
0012 COMMON/L11/ THC(30),HC(30),CAPC(30)
0013 COMMON/L12/ AC,BC,NX,NA1,CONST
0014 COMMON/L13/ WFLUX(810)
0015 COMMON/L14/ VO,TWO,TSALT
0016 100 FORMAT(SX,'TIME ,HOURS =',F10.5/,
* SX,'LENGTH OF SOIL PROFILE, CM=',F10.5/,
* SX,'VOLUME OF WATER IN THE SOIL PROFILE, CM =',F10.5/)
0017 200 FORMAT(SX,'TOTAL NH-4 IN EXCH. PHASE, MG =',F10.5/,
* SX,'TOTAL NH-4 IN SOIL SOLUTION PHASE, MG =',F10.5/,
* SX,'TOTAL NH-4 IN SOIL, MG =',F10.5/)
0018 300 FORMAT(SX,'TOTAL NH-3 IN SOIL SOLUTION, MG =',F10.5/,
* SX,'TOTAL ORGANIC N IN THE SOIL, MG =',F10.5/,
* SX,'TOTAL NO-2 RELEASED FROM THE SOIL, MG =',F10.5//)
C
0019 DO 5 I=1,NP1
0020 X(I)=TH(I)*CNH4(I)
0021 5 CONTINUE
0022 CALL QSF(DZ,X,AA,NP1)
0023 TNH4C=AA(NP1)
0024 CALL QSF(DZ,CNH4,AA,NP1)
0025 TNH4SS=AA(NP1)*ROU*RKD
0026 TNH4T=TNH4C+TNH4SS
C
0027 DO 10 I=1,NP1
0028 X(I)=TH(I)*CNO3(I)
0029 10 CONTINUE
0030 CALL QSF(DZ,X,AA,NP1)
0031 TNH3=AA(NP1)
C
0032 DO 15 I=1,NP1
0033 X(I)=ROU*CORGN(I)
0034 15 CONTINUE
0035 CALL QSF(DZ,X,AA,NP1)
0036 TORGN=AA(NP1)
C
0037 CALL QSF(DZ,TH,AA,NP1)
0038 TW=AA(NP1)
0039 DO 20 I=1,NP2
0040 X(I)=ROU*CNO2(I)
0041 20 CONTINUE
0042 CALL QSF(DZ,X,AA,NP1)
0043 TGASN=AA(NP1)
0044 CL=N*DZ
0045 WRITE(6,100) TIME,CL,TW
0046 WRITE(6,200) TNH4SS, TNH4C, TNH4T
0047 WRITE(6,300) TNH3, TORGN, TGASN
C
0048 CALL SBCW
0049 RETURN
0050 END

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0001      C      *****
0002      C      SUBROUTINE TRIDM(A,B,C,D,X,N)
0003      C      DIMENSION A(1),B(1),C(1),D(1),X(1)
0004      C      DO 1 I=2,N
0005      C      C(I-1)=C(I-1)/A(I-1)
0006      C      A(I)=A(I)-(C(I-1)*B(I-1))
0007      C      1 CONTINUE
0008      C      X(1)=D(1)
0009      C      DO 2 I=2,N
0010      C      X(I)=D(I)-(C(I-1)*X(I-1))
0011      C      2 CONTINUE
0012      C      X(N)=X(N)/A(N)
0013      C      DO 3 I=2,N
0014      C      X(N+1-I)=(X(N+1-I)-(B(N+1-I)*X(N+2-I)))/A(N+1-I)
0015      C      3 CONTINUE
0016      C      RETURN
0017      C      END

```

94-SELIMX -GQ -FT06F001

| | | | | | | | |
|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|
| 0.3600 | 0.3500 | 0.3400 | 0.3300 | 0.3200 | 0.3100 | 0.3000 | 0.2900 |
| 0.2800 | 0.2700 | 0.2600 | 0.2500 | 0.2400 | 0.2300 | 0.2200 | 0.2100 |
| 0.2000 | 0.1900 | 0.1800 | 0.1700 | 0.1600 | 0.1500 | 0.1400 | 0.1300 |
| 0.0 | -22.0000 | -31.0000 | -43.0000 | -58.0000 | -75.0000 | -95.0000 | -115.0000 |
| -138.0000 | -159.0000 | -179.0000 | -200.0000 | -229.0000 | -262.0000 | -300.0000 | -350.0000 |
| -415.0000 | -495.0000 | -595.0000 | -720.0000 | -900.0000 | -1180.0000 | -1530.0000 | -2000.0000 |
| 1.0000 | 0.0000 | 0.0000 | 0.2200 | -300.0000 | 20.0000 | 0.0 | |
| 1.0000 | 0.3600 | 0.2200 | -300.0000 | 20.0000 | 0.0 | | |
| 100.0000 | 1.6000 | 100.0000 | 100.0000 | | | | |
| .1800E-10 | .6560E-02 | .3500E-00 | | | | | |
| 1.0000 | 2.0000 | 5.0000 | 10.0000 | | | | |
| 0.1000 | 0.1000 | 0.0001 | 0.0010 | 0.0010 | 0.0 | | |
| 0.0 | 10.0000 | 100.0000 | | | | | |
| -300.0000 | -300.0000 | -300.0000 | | | | | |
| 0.2200 | 0.2200 | 0.2200 | | | | | |
| 0.0 | 0.0 | 0.0 | | | | | |
| 0.0 | 0.0 | 0.0 | | | | | |
| 20.0000 | 20.0000 | 20.0000 | | | | | |
| 0.0 | 0.0 | 0.0 | | | | | |

$$\text{Time} = 0.10000 \text{ s}$$

| DEPTH, CM | SUCTION, CM | THEIA | HYD2, COND. | WATER FLUX | NH4 | NH3 | CO2, EGN |
|-----------|-------------|--------|-------------|------------|---------|---------|----------|
| 0.0 | 0.0 | 0.3500 | 0.3213 | 0.1141F | 0.0095E | 0.1005E | 0.2000E |
| 0.0 | 0.3189E | 0.3599 | 0.3202 | 0.1141F | 0.0095E | 0.1006E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.3171E | 0.1141F | 0.0095E | 0.1010E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.3140E | 0.1141F | 0.0095E | 0.1014E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.3109E | 0.1141F | 0.0095E | 0.1014E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.3078E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.3047E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.3016E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2985E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2954E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2923E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2892E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2861E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2830E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2799E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2768E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2737E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2706E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2675E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2644E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2613E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2582E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2551E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2520E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2489E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2458E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2427E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2396E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2365E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2334E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2303E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2272E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2241E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2210E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2179E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2148E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2117E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2086E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2055E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.2024E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1993E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1962E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1931E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1900E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1869E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1838E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1807E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1776E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1745E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1714E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1683E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1652E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1621E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1590E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1559E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1528E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1497E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1466E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1435E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1404E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1373E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1342E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1311E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1280E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1249E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1218E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1187E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1156E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1125E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1094E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1063E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1032E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.1001E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0970E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0939E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0908E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0877E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0846E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0815E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0784E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0753E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0722E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0691E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0660E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0629E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0598E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0567E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0536E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0505E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0474E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0443E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0412E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0381E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0350E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0319E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0288E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0257E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0226E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0195E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0164E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0133E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0102E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0071E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0040E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0009E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |
| 0.0 | 0.3599 | 0.3599 | 0.0000E | 0.1141F | 0.0095E | 0.1015E | 0.2000E |

[illegible]

LENGTH OF SOIL PROFILE, CM = 13.12500
VOLUME OF WATER IN THE SOIL PROFILE, CM = 4.06647

TOTAL NH-4 IN EXCH. PHASE, MG = 31.36497
TOTAL NH-4 IN SOIL SOLUTION PHASE, MG = 70.23523
TOTAL NH-4 IN SOIL, MG = 101.58020

TOTAL NH-3 IN SOIL SOLUTION, MG = 107.69272
TOTAL ORGANIC N IN THE SOIL, MG = 419.77100
TOTAL NC-2 RELEASED FROM THE SOIL, MG = 0.0

| DEPTH, CM | SUCTION, CM | THETA | HYDR. COND. | TIME | WATER FLUX | NO ₄ | CURGN | NO ₃ | NO ₂ |
|-----------|-------------|---------|-------------|------|------------|-----------------|---------|-----------------|-----------------|
| 0.0 | 0.0 | 0.3509F | 0.3221F | 00 | 0.7387F | 0.0920F | 0.2000F | 0.1003F | 0.0 |
| 0.1250E | -0.1617E | 0.3569F | 0.3274F | 00 | 0.7387F | 0.0920F | 0.2000F | 0.1014F | 0.0 |
| 0.2500E | -0.2231E | 0.3559F | 0.3205F | 00 | 0.7387E | 0.0920F | 0.2000E | 0.1019E | 0.0 |
| 0.3750E | -0.2558E | 0.3558F | 0.3193F | 00 | 0.7386E | 0.0920F | 0.2000E | 0.1025E | 0.0 |
| 0.5000E | -0.2660E | 0.3557F | 0.3177F | 00 | 0.7386E | 0.0920F | 0.2000E | 0.1030E | 0.0 |
| 0.6250E | -0.2660E | 0.3556F | 0.3177F | 00 | 0.7386E | 0.0920F | 0.2000E | 0.1030E | 0.0 |
| 0.7500E | -0.2660E | 0.3555F | 0.3177F | 00 | 0.7385E | 0.0920F | 0.1999F | 0.1030E | 0.0 |
| 0.8750E | -0.2660E | 0.3554F | 0.3130F | 00 | 0.7385E | 0.0920F | 0.1999F | 0.1040E | 0.0 |
| 0.1000F | -0.1151E | 0.3554F | 0.3130F | 00 | 0.7385E | 0.0920F | 0.1999F | 0.1045F | 0.0 |
| 0.1125E | -0.1493E | 0.3553F | 0.3068F | 00 | 0.7384E | 0.0920F | 0.1999F | 0.1045F | 0.0 |
| 0.1250E | -0.1655E | 0.3552F | 0.3068F | 00 | 0.7384E | 0.0920F | 0.1999F | 0.1055E | 0.0 |
| 0.1375E | -0.1740E | 0.3552F | 0.3066F | 00 | 0.7384E | 0.0920F | 0.1999F | 0.1055E | 0.0 |
| 0.1500E | -0.1801E | 0.3551F | 0.3066F | 00 | 0.7383E | 0.0920F | 0.1999F | 0.1063E | 0.0 |
| 0.1625E | -0.1843E | 0.3550F | 0.3033F | 00 | 0.7382E | 0.0920F | 0.1999F | 0.1071E | 0.0 |
| 0.1750E | -0.1873E | 0.3549F | 0.3017F | 00 | 0.7382E | 0.0920F | 0.1999F | 0.1071E | 0.0 |
| 0.1875E | -0.1873E | 0.3548F | 0.3012F | 00 | 0.7380E | 0.0920F | 0.1999F | 0.1077E | 0.0 |
| 0.2000E | -0.1873E | 0.3548F | 0.2994F | 00 | 0.7380E | 0.0920F | 0.1999F | 0.1077E | 0.0 |
| 0.2125E | -0.1873E | 0.3547F | 0.2994F | 00 | 0.7379E | 0.0920F | 0.1999F | 0.1080E | 0.0 |
| 0.2250E | -0.1873E | 0.3546F | 0.2964F | 00 | 0.7378E | 0.0920F | 0.1999F | 0.1092E | 0.0 |
| 0.2375E | -0.1873E | 0.3545F | 0.2964F | 00 | 0.7378E | 0.0920F | 0.1999F | 0.1092E | 0.0 |
| 0.2500E | -0.1873E | 0.3544F | 0.2935E | 00 | 0.7377E | 0.0920F | 0.1997E | 0.1094E | 0.0 |
| 0.2625E | -0.1873E | 0.3543F | 0.2935E | 00 | 0.7376E | 0.0920F | 0.1997E | 0.1093E | 0.0 |
| 0.2750E | -0.1873E | 0.3542F | 0.2902E | 00 | 0.7375E | 0.0920F | 0.1997E | 0.1082E | 0.0 |
| 0.2875E | -0.1873E | 0.3541F | 0.2885F | 00 | 0.7374E | 0.0920F | 0.1997E | 0.1080E | 0.0 |
| 0.3000E | -0.1873E | 0.3540F | 0.2885F | 00 | 0.7373E | 0.0920F | 0.1997E | 0.1076E | 0.0 |
| 0.3125E | -0.1873E | 0.3539F | 0.2851E | 00 | 0.7371E | 0.0920F | 0.1997E | 0.1071E | 0.0 |
| 0.3250E | -0.1873E | 0.3538F | 0.2851E | 00 | 0.7371E | 0.0920F | 0.1997E | 0.1071E | 0.0 |
| 0.3375E | -0.1873E | 0.3537F | 0.2837E | 00 | 0.7370E | 0.0920F | 0.1997E | 0.1064E | 0.0 |
| 0.3500E | -0.1873E | 0.3536F | 0.2837E | 00 | 0.7369E | 0.0920F | 0.1997E | 0.1064E | 0.0 |
| 0.3625E | -0.1873E | 0.3535F | 0.2823E | 00 | 0.7367E | 0.0920F | 0.1997E | 0.1044E | 0.0 |
| 0.3750E | -0.1873E | 0.3534F | 0.2823E | 00 | 0.7366E | 0.0920F | 0.1997E | 0.1044E | 0.0 |
| 0.3875E | -0.1873E | 0.3533F | 0.2782E | 00 | 0.7364E | 0.0920F | 0.1996E | 0.1015E | 0.0 |
| 0.4000E | -0.1873E | 0.3532F | 0.2782E | 00 | 0.7363E | 0.0920F | 0.1996E | 0.1015E | 0.0 |
| 0.4125E | -0.1873E | 0.3531F | 0.2731E | 00 | 0.7362E | 0.0920F | 0.1996E | 0.0956E | 0.0 |
| 0.4250E | -0.1873E | 0.3530F | 0.2731E | 00 | 0.7362E | 0.0920F | 0.1996E | 0.0956E | 0.0 |
| 0.4375E | -0.1873E | 0.3529F | 0.2714E | 00 | 0.7362E | 0.0920F | 0.1996E | 0.0956E | 0.0 |
| 0.4500E | -0.1873E | 0.3528F | 0.2697E | 00 | 0.7358E | 0.0920F | 0.1996E | 0.09251E | 0.0 |
| 0.4625E | -0.1873E | 0.3527E | 0.2697E | 00 | 0.7358E | 0.0920F | 0.1996E | 0.0957E | 0.0 |
| 0.4750E | -0.1873E | 0.3526F | 0.2652E | 00 | 0.7354E | 0.0920F | 0.1996E | 0.0957E | 0.0 |
| 0.4875E | -0.1873E | 0.3525F | 0.2652E | 00 | 0.7354E | 0.0920F | 0.1996E | 0.0957E | 0.0 |
| 0.5000E | -0.1873E | 0.3524F | 0.2644E | 00 | 0.7352E | 0.0920F | 0.1996E | 0.09287E | 0.0 |
| 0.5125E | -0.1873E | 0.3523F | 0.2627E | 00 | 0.7350F | 0.0920F | 0.1996E | 0.09714E | 0.0 |
| 0.5250E | -0.1873E | 0.3522F | 0.2609E | 00 | 0.7347F | 0.0920F | 0.1996E | 0.09714E | 0.0 |
| 0.5375E | -0.1873E | 0.3521F | 0.2591E | 00 | 0.7343F | 0.0920F | 0.1996E | 0.09714E | 0.0 |
| 0.5500E | -0.1873E | 0.3520F | 0.2573E | 00 | 0.7333F | 0.0920F | 0.1996E | 0.09714E | 0.0 |
| 0.5625E | -0.1873E | 0.3519E | 0.2555E | 00 | 0.7331E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.5750E | -0.1873E | 0.3518E | 0.2538E | 00 | 0.7335E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.5875E | -0.1873E | 0.3517E | 0.2520E | 00 | 0.7335E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.6000E | -0.1873E | 0.3516E | 0.2502E | 00 | 0.7332E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.6125E | -0.1873E | 0.3515E | 0.2483E | 00 | 0.7330F | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.6250E | -0.1873E | 0.3514E | 0.2465E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.6375E | -0.1873E | 0.3513E | 0.2447E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.6500E | -0.1873E | 0.3512E | 0.2429E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.6625E | -0.1873E | 0.3511E | 0.2411E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.6750E | -0.1873E | 0.3510E | 0.2392E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.6875E | -0.1873E | 0.3509E | 0.2374E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.7000E | -0.1873E | 0.3508E | 0.2356E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.7125E | -0.1873E | 0.3507E | 0.2338E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.7250E | -0.1873E | 0.3506E | 0.2320E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.7375E | -0.1873E | 0.3505E | 0.2302E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.7500E | -0.1873E | 0.3504E | 0.2284E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.7625E | -0.1873E | 0.3503E | 0.2266E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.7750E | -0.1873E | 0.3502E | 0.2248E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.7875E | -0.1873E | 0.3501E | 0.2230E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.8000E | -0.1873E | 0.3500E | 0.2212E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.8125E | -0.1873E | 0.3499E | 0.2194E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.8250E | -0.1873E | 0.3498E | 0.2176E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.8375E | -0.1873E | 0.3497E | 0.2158E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.8500E | -0.1873E | 0.3496E | 0.2140E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.8625E | -0.1873E | 0.3495E | 0.2122E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.8750E | -0.1873E | 0.3494E | 0.2104E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.8875E | -0.1873E | 0.3493E | 0.2086E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.9000E | -0.1873E | 0.3492E | 0.2068E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.9125E | -0.1873E | 0.3491E | 0.2050E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.9250E | -0.1873E | 0.3490E | 0.2032E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.9375E | -0.1873E | 0.3489E | 0.2014E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.9500E | -0.1873E | 0.3488E | 0.1996E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.9625E | -0.1873E | 0.3487E | 0.1978E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.9750E | -0.1873E | 0.3486E | 0.1960E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.9875E | -0.1873E | 0.3485E | 0.1942E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 1.0000E | -0.1873E | 0.3484E | 0.1924E | 00 | 0.7329E | 0.0920F | 0.1996E | 0.09210E | 0.0 |
| 0.0 | 0.0 | 0.3509F | 0.3221F | 00 | 0.7387F | 0.0920F | 0.2000F | 0.1003F | 0.0 |
| 0.1250E | -0.1617E | 0.3569F | 0.3274F | 00 | 0.7387F | 0.0920F | 0.2000F | 0.1014F | 0.0 |
| 0.2500E | -0.2231E | 0.3559F | 0.3205F | 00 | 0.7387E | 0.0920F | 0.2000E | 0.1019E | 0.0 |
| 0.3750E | -0.2558E | 0.3558F | 0.3193F | 00 | 0.7386E | 0.0920F | 0.2000E | 0.1025E | 0.0 |
| 0.5000E | -0.2660E | 0.3557F | 0.3177F | 00 | 0.7386E | 0.0920F | 0.2000E | 0.1030E | 0.0 |
| 0.6250E | -0.2660E | 0.3556F | 0.3177F | 00 | 0.7386E | 0.0920F | 0.2000E | 0.1030E | 0.0 |
| 0.7500E | -0.2660E | 0.3555F | 0.3177F | 00 | 0.7385E | 0.0920F | 0.1999F | 0.1030E | 0.0 |
| 0.8750E | -0.2660E | 0.3554F | 0.3130F | 00 | 0.7385E | 0.0920F | 0.1999F | 0.1040E | 0.0 |
| 0.1000F | -0.1151E | 0.3554F | 0.3130F | 00 | 0.7385E | 0.0920F | 0.1999F | 0.1045F | 0.0 |
| 0.1125E | -0.1493E | 0.3553F | 0.3068F | 00 | 0.7384E | 0.0920F | 0.1999F | 0.1045F | 0.0 |
| 0.1250E | -0.1655E | 0.3552F | 0.3068F | 00 | 0.7384E | 0.0920F | 0.1999F | 0.1055E | 0.0 |
| 0.1375E | -0.1740E | 0.3552F | 0.3066F | 00 | 0.7384E | 0.0920F | 0.1999F | 0.1055E | 0.0 |
| 0.1500E | -0.1801E | 0.3551F | 0.3066F | 00 | 0.7383E | 0.0920F | 0.1999F | 0.1063E | 0.0 |
| 0.1625E | -0.1843E | 0.3550F | 0.3033F | 00 | 0.7382E | 0.0920F | 0.1999F | 0.1071E | 0.0 |
| 0.1750E | -0.1873E | 0.3549F | 0.3017F | 00 | 0.7382E | 0.0920F | 0.1999F | 0.1071E | 0.0 |
| 0.1875E | -0.1873E | 0.3548F | 0.3012F | 00 | 0.7380E | 0.0920F | 0.1999F | 0.1077E | 0.0 |
| 0.2000E | -0.1873E | 0.3548F | 0.2994F | 00 | 0.7380E | 0.0920F | 0.1999F | 0.1077E | 0.0 |
| 0.2125E | -0.1873E | 0.3547F | 0.2994F | 00 | 0.7379E | 0.0920F | 0.1999F | 0.1080E | 0.0 |
| 0.2250E | -0.1873E | 0.3546F | 0.2964F | 00 | 0.7378E | 0.0920F | 0.1999F | 0.1092E | 0.0 |
| 0.2375E | -0.1873E | 0.3545F | 0.2964F | 00 | 0.7378E | 0.0920F | 0.1999F | 0.1092E | 0.0 |
| 0.2500E | -0.1873E | 0.3544F | 0.2935E | 00 | 0.7377E | 0.0920F | 0.1997E | 0.1094E | 0.0 |
| 0.2625E | -0.1873E | 0.3543F | 0.2935E | 00 | 0.7376E | 0.0920F | 0.1997E | 0.1093E | 0.0 |
| 0.2750E | -0.1873E | 0.3542F | 0.2902E | 00 | 0.7375E | 0.0920F | 0.1997E | 0.1082E | 0.0 |
| 0.2875E | -0.1873E | 0.3541F | 0.2885F | 00 | 0.7374E | 0.0920F | 0.1997E | 0.1080E | 0.0 |
| 0.3000E | -0.1873E | 0.3540F | 0.2885F | 00 | 0.7373E | 0.0920F | 0.1997E | 0.1076E | 0.0 |
| 0.3125E | -0.1873E | 0.3539F | 0.2851E | 00 | 0.7371E | | | | |

| | | | | | | | | |
|--------|---------|--------|--------|--------|--------|--------|--------|-----|
| 0.0620 | 0.1819 | 0.3517 | 0.1875 | 0.7194 | 0.8021 | 0.3331 | 0.1997 | 0.0 |
| 0.0750 | -0.1855 | 0.3516 | 0.1855 | 0.7173 | 0.8256 | 0.2483 | 0.1997 | 0.0 |
| 0.0900 | -0.1895 | 0.3514 | 0.1855 | 0.7171 | 0.8435 | 0.1915 | 0.1997 | 0.0 |
| 0.1000 | -0.1925 | 0.3512 | 0.1855 | 0.7174 | 0.8634 | 0.1401 | 0.1997 | 0.0 |
| 0.1100 | -0.1955 | 0.3510 | 0.1855 | 0.7176 | 0.8857 | 0.1100 | 0.1997 | 0.0 |
| 0.1200 | -0.1985 | 0.3508 | 0.1855 | 0.7178 | 0.9100 | 0.0900 | 0.1997 | 0.0 |
| 0.1300 | -0.2015 | 0.3506 | 0.1855 | 0.7180 | 0.9362 | 0.0700 | 0.1997 | 0.0 |
| 0.1400 | -0.2045 | 0.3504 | 0.1855 | 0.7182 | 0.9643 | 0.0500 | 0.1997 | 0.0 |
| 0.1500 | -0.2075 | 0.3502 | 0.1855 | 0.7184 | 0.9943 | 0.0300 | 0.1997 | 0.0 |
| 0.1600 | -0.2105 | 0.3500 | 0.1855 | 0.7186 | 1.0262 | 0.0100 | 0.1997 | 0.0 |
| 0.1700 | -0.2135 | 0.3498 | 0.1855 | 0.7188 | 1.0600 | 0.0000 | 0.1997 | 0.0 |
| 0.1800 | -0.2165 | 0.3496 | 0.1855 | 0.7190 | 1.0957 | 0.0000 | 0.1997 | 0.0 |
| 0.1900 | -0.2195 | 0.3494 | 0.1855 | 0.7192 | 1.1333 | 0.0000 | 0.1997 | 0.0 |
| 0.2000 | -0.2225 | 0.3492 | 0.1855 | 0.7194 | 1.1728 | 0.0000 | 0.1997 | 0.0 |
| 0.2100 | -0.2255 | 0.3490 | 0.1855 | 0.7196 | 1.2141 | 0.0000 | 0.1997 | 0.0 |
| 0.2200 | -0.2285 | 0.3488 | 0.1855 | 0.7198 | 1.2572 | 0.0000 | 0.1997 | 0.0 |
| 0.2300 | -0.2315 | 0.3486 | 0.1855 | 0.7200 | 1.3021 | 0.0000 | 0.1997 | 0.0 |
| 0.2400 | -0.2345 | 0.3484 | 0.1855 | 0.7202 | 1.3488 | 0.0000 | 0.1997 | 0.0 |
| 0.2500 | -0.2375 | 0.3482 | 0.1855 | 0.7204 | 1.3972 | 0.0000 | 0.1997 | 0.0 |
| 0.2600 | -0.2405 | 0.3480 | 0.1855 | 0.7206 | 1.4473 | 0.0000 | 0.1997 | 0.0 |
| 0.2700 | -0.2435 | 0.3478 | 0.1855 | 0.7208 | 1.4990 | 0.0000 | 0.1997 | 0.0 |
| 0.2800 | -0.2465 | 0.3476 | 0.1855 | 0.7210 | 1.5523 | 0.0000 | 0.1997 | 0.0 |
| 0.2900 | -0.2495 | 0.3474 | 0.1855 | 0.7212 | 1.6072 | 0.0000 | 0.1997 | 0.0 |
| 0.3000 | -0.2525 | 0.3472 | 0.1855 | 0.7214 | 1.6637 | 0.0000 | 0.1997 | 0.0 |
| 0.3100 | -0.2555 | 0.3470 | 0.1855 | 0.7216 | 1.7218 | 0.0000 | 0.1997 | 0.0 |
| 0.3200 | -0.2585 | 0.3468 | 0.1855 | 0.7218 | 1.7815 | 0.0000 | 0.1997 | 0.0 |
| 0.3300 | -0.2615 | 0.3466 | 0.1855 | 0.7220 | 1.8428 | 0.0000 | 0.1997 | 0.0 |
| 0.3400 | -0.2645 | 0.3464 | 0.1855 | 0.7222 | 1.9057 | 0.0000 | 0.1997 | 0.0 |
| 0.3500 | -0.2675 | 0.3462 | 0.1855 | 0.7224 | 1.9702 | 0.0000 | 0.1997 | 0.0 |
| 0.3600 | -0.2705 | 0.3460 | 0.1855 | 0.7226 | 2.0363 | 0.0000 | 0.1997 | 0.0 |
| 0.3700 | -0.2735 | 0.3458 | 0.1855 | 0.7228 | 2.1040 | 0.0000 | 0.1997 | 0.0 |
| 0.3800 | -0.2765 | 0.3456 | 0.1855 | 0.7230 | 2.1733 | 0.0000 | 0.1997 | 0.0 |
| 0.3900 | -0.2795 | 0.3454 | 0.1855 | 0.7232 | 2.2442 | 0.0000 | 0.1997 | 0.0 |
| 0.4000 | -0.2825 | 0.3452 | 0.1855 | 0.7234 | 2.3167 | 0.0000 | 0.1997 | 0.0 |
| 0.4100 | -0.2855 | 0.3450 | 0.1855 | 0.7236 | 2.3908 | 0.0000 | 0.1997 | 0.0 |
| 0.4200 | -0.2885 | 0.3448 | 0.1855 | 0.7238 | 2.4665 | 0.0000 | 0.1997 | 0.0 |
| 0.4300 | -0.2915 | 0.3446 | 0.1855 | 0.7240 | 2.5438 | 0.0000 | 0.1997 | 0.0 |
| 0.4400 | -0.2945 | 0.3444 | 0.1855 | 0.7242 | 2.6227 | 0.0000 | 0.1997 | 0.0 |
| 0.4500 | -0.2975 | 0.3442 | 0.1855 | 0.7244 | 2.7032 | 0.0000 | 0.1997 | 0.0 |
| 0.4600 | -0.3005 | 0.3440 | 0.1855 | 0.7246 | 2.7853 | 0.0000 | 0.1997 | 0.0 |
| 0.4700 | -0.3035 | 0.3438 | 0.1855 | 0.7248 | 2.8690 | 0.0000 | 0.1997 | 0.0 |
| 0.4800 | -0.3065 | 0.3436 | 0.1855 | 0.7250 | 2.9543 | 0.0000 | 0.1997 | 0.0 |
| 0.4900 | -0.3095 | 0.3434 | 0.1855 | 0.7252 | 3.0412 | 0.0000 | 0.1997 | 0.0 |
| 0.5000 | -0.3125 | 0.3432 | 0.1855 | 0.7254 | 3.1297 | 0.0000 | 0.1997 | 0.0 |
| 0.5100 | -0.3155 | 0.3430 | 0.1855 | 0.7256 | 3.2198 | 0.0000 | 0.1997 | 0.0 |
| 0.5200 | -0.3185 | 0.3428 | 0.1855 | 0.7258 | 3.3115 | 0.0000 | 0.1997 | 0.0 |
| 0.5300 | -0.3215 | 0.3426 | 0.1855 | 0.7260 | 3.4048 | 0.0000 | 0.1997 | 0.0 |
| 0.5400 | -0.3245 | 0.3424 | 0.1855 | 0.7262 | 3.5000 | 0.0000 | 0.1997 | 0.0 |
| 0.5500 | -0.3275 | 0.3422 | 0.1855 | 0.7264 | 3.5968 | 0.0000 | 0.1997 | 0.0 |
| 0.5600 | -0.3305 | 0.3420 | 0.1855 | 0.7266 | 3.6953 | 0.0000 | 0.1997 | 0.0 |
| 0.5700 | -0.3335 | 0.3418 | 0.1855 | 0.7268 | 3.7954 | 0.0000 | 0.1997 | 0.0 |
| 0.5800 | -0.3365 | 0.3416 | 0.1855 | 0.7270 | 3.8971 | 0.0000 | 0.1997 | 0.0 |
| 0.5900 | -0.3395 | 0.3414 | 0.1855 | 0.7272 | 4.0005 | 0.0000 | 0.1997 | 0.0 |
| 0.6000 | -0.3425 | 0.3412 | 0.1855 | 0.7274 | 4.1055 | 0.0000 | 0.1997 | 0.0 |
| 0.6100 | -0.3455 | 0.3410 | 0.1855 | 0.7276 | 4.2121 | 0.0000 | 0.1997 | 0.0 |
| 0.6200 | -0.3485 | 0.3408 | 0.1855 | 0.7278 | 4.3203 | 0.0000 | 0.1997 | 0.0 |
| 0.6300 | -0.3515 | 0.3406 | 0.1855 | 0.7280 | 4.4301 | 0.0000 | 0.1997 | 0.0 |
| 0.6400 | -0.3545 | 0.3404 | 0.1855 | 0.7282 | 4.5415 | 0.0000 | 0.1997 | 0.0 |
| 0.6500 | -0.3575 | 0.3402 | 0.1855 | 0.7284 | 4.6545 | 0.0000 | 0.1997 | 0.0 |
| 0.6600 | -0.3605 | 0.3400 | 0.1855 | 0.7286 | 4.7691 | 0.0000 | 0.1997 | 0.0 |
| 0.6700 | -0.3635 | 0.3398 | 0.1855 | 0.7288 | 4.8853 | 0.0000 | 0.1997 | 0.0 |
| 0.6800 | -0.3665 | 0.3396 | 0.1855 | 0.7290 | 5.0031 | 0.0000 | 0.1997 | 0.0 |
| 0.6900 | -0.3695 | 0.3394 | 0.1855 | 0.7292 | 5.1225 | 0.0000 | 0.1997 | 0.0 |
| 0.7000 | -0.3725 | 0.3392 | 0.1855 | 0.7294 | 5.2435 | 0.0000 | 0.1997 | 0.0 |
| 0.7100 | -0.3755 | 0.3390 | 0.1855 | 0.7296 | 5.3661 | 0.0000 | 0.1997 | 0.0 |
| 0.7200 | -0.3785 | 0.3388 | 0.1855 | 0.7298 | 5.4903 | 0.0000 | 0.1997 | 0.0 |
| 0.7300 | -0.3815 | 0.3386 | 0.1855 | 0.7300 | 5.6161 | 0.0000 | 0.1997 | 0.0 |
| 0.7400 | -0.3845 | 0.3384 | 0.1855 | 0.7302 | 5.7435 | 0.0000 | 0.1997 | 0.0 |
| 0.7500 | -0.3875 | 0.3382 | 0.1855 | 0.7304 | 5.8725 | 0.0000 | 0.1997 | 0.0 |
| 0.7600 | -0.3905 | 0.3380 | 0.1855 | 0.7306 | 6.0031 | 0.0000 | 0.1997 | 0.0 |
| 0.7700 | -0.3935 | 0.3378 | 0.1855 | 0.7308 | 6.1353 | 0.0000 | 0.1997 | 0.0 |
| 0.7800 | -0.3965 | 0.3376 | 0.1855 | 0.7310 | 6.2691 | 0.0000 | 0.1997 | 0.0 |
| 0.7900 | -0.3995 | 0.3374 | 0.1855 | 0.7312 | 6.4045 | 0.0000 | 0.1997 | 0.0 |
| 0.8000 | -0.4025 | 0.3372 | 0.1855 | 0.7314 | 6.5415 | 0.0000 | 0.1997 | 0.0 |
| 0.8100 | -0.4055 | 0.3370 | 0.1855 | 0.7316 | 6.6801 | 0.0000 | 0.1997 | 0.0 |
| 0.8200 | -0.4085 | 0.3368 | 0.1855 | 0.7318 | 6.8203 | 0.0000 | 0.1997 | 0.0 |
| 0.8300 | -0.4115 | 0.3366 | 0.1855 | 0.7320 | 6.9621 | 0.0000 | 0.1997 | 0.0 |
| 0.8400 | -0.4145 | 0.3364 | 0.1855 | 0.7322 | 7.1055 | 0.0000 | 0.1997 | 0.0 |
| 0.8500 | -0.4175 | 0.3362 | 0.1855 | 0.7324 | 7.2505 | 0.0000 | 0.1997 | 0.0 |
| 0.8600 | -0.4205 | 0.3360 | 0.1855 | 0.7326 | 7.3971 | 0.0000 | 0.1997 | 0.0 |
| 0.8700 | -0.4235 | 0.3358 | 0.1855 | 0.7328 | 7.5453 | 0.0000 | 0.1997 | 0.0 |
| 0.8800 | -0.4265 | 0.3356 | 0.1855 | 0.7330 | 7.6951 | 0.0000 | 0.1997 | 0.0 |
| 0.8900 | -0.4295 | 0.3354 | 0.1855 | 0.7332 | 7.8465 | 0.0000 | 0.1997 | 0.0 |
| 0.9000 | -0.4325 | 0.3352 | 0.1855 | 0.7334 | 7.9995 | 0.0000 | 0.1997 | 0.0 |
| 0.9100 | -0.4355 | 0.3350 | 0.1855 | 0.7336 | 8.1541 | 0.0000 | 0.1997 | 0.0 |
| 0.9200 | -0.4385 | 0.3348 | 0.1855 | 0.7338 | 8.3103 | 0.0000 | 0.1997 | 0.0 |
| 0.9300 | -0.4415 | 0.3346 | 0.1855 | 0.7340 | 8.4681 | 0.0000 | 0.1997 | 0.0 |
| 0.9400 | -0.4445 | 0.3344 | 0.1855 | 0.7342 | 8.6275 | 0.0000 | 0.1997 | 0.0 |
| 0.9500 | -0.4475 | 0.3342 | 0.1855 | 0.7344 | 8.7885 | 0.0000 | 0.1997 | 0.0 |
| 0.9600 | -0.4505 | 0.3340 | 0.1855 | 0.7346 | 8.9511 | 0.0000 | 0.1997 | 0.0 |
| 0.9700 | -0.4535 | 0.3338 | 0.1855 | 0.7348 | 9.1153 | 0.0000 | 0.1997 | 0.0 |
| 0.9800 | -0.4565 | 0.3336 | 0.1855 | 0.7350 | 9.2811 | 0.0000 | 0.1997 | 0.0 |
| 0.9900 | -0.4595 | 0.3334 | 0.1855 | 0.7352 | 9.4485 | 0.0000 | 0.1997 | 0.0 |
| 1.0000 | -0.4625 | 0.3332 | 0.1855 | 0.7354 | 9.6175 | 0.0000 | 0.1997 | 0.0 |

TIME, HOURS = 2.0000
 LENGTH OF SOIL PROFILE, CM = 19.37500
 VOLUME OF WATER IN THE SOIL PROFILE, CM = 6.3442
 TOTAL NH-4 IN EXCH. PHASE, MG = 55.6361

TOTAL NH-4 IN SCIL SOLUTION PHASE, MG = 124.72713
TOTAL NH-4 IN SCIL, MG = 180.36394

TOTAL NH-4 IN SCIL SOLUTION, MG = 206.42267
TOTAL ORGANIC N IN THE SCIL, MG = 615.9301
TOTAL NH₄ RELEASED FROM THE SCIL, MG = 0.0

| TIME | 0.000000 | 01 |
|------|----------|----------|
| 0.0 | 0.000000 | 0.000000 |
| 0.1 | 0.000000 | 0.000000 |
| 0.2 | 0.000000 | 0.000000 |
| 0.3 | 0.000000 | 0.000000 |
| 0.4 | 0.000000 | 0.000000 |
| 0.5 | 0.000000 | 0.000000 |
| 0.6 | 0.000000 | 0.000000 |
| 0.7 | 0.000000 | 0.000000 |
| 0.8 | 0.000000 | 0.000000 |
| 0.9 | 0.000000 | 0.000000 |
| 1.0 | 0.000000 | 0.000000 |
| 1.1 | 0.000000 | 0.000000 |
| 1.2 | 0.000000 | 0.000000 |
| 1.3 | 0.000000 | 0.000000 |
| 1.4 | 0.000000 | 0.000000 |
| 1.5 | 0.000000 | 0.000000 |
| 1.6 | 0.000000 | 0.000000 |
| 1.7 | 0.000000 | 0.000000 |
| 1.8 | 0.000000 | 0.000000 |
| 1.9 | 0.000000 | 0.000000 |
| 2.0 | 0.000000 | 0.000000 |
| 2.1 | 0.000000 | 0.000000 |
| 2.2 | 0.000000 | 0.000000 |
| 2.3 | 0.000000 | 0.000000 |
| 2.4 | 0.000000 | 0.000000 |
| 2.5 | 0.000000 | 0.000000 |
| 2.6 | 0.000000 | 0.000000 |
| 2.7 | 0.000000 | 0.000000 |
| 2.8 | 0.000000 | 0.000000 |
| 2.9 | 0.000000 | 0.000000 |
| 3.0 | 0.000000 | 0.000000 |
| 3.1 | 0.000000 | 0.000000 |
| 3.2 | 0.000000 | 0.000000 |
| 3.3 | 0.000000 | 0.000000 |
| 3.4 | 0.000000 | 0.000000 |
| 3.5 | 0.000000 | 0.000000 |
| 3.6 | 0.000000 | 0.000000 |
| 3.7 | 0.000000 | 0.000000 |
| 3.8 | 0.000000 | 0.000000 |
| 3.9 | 0.000000 | 0.000000 |
| 4.0 | 0.000000 | 0.000000 |
| 4.1 | 0.000000 | 0.000000 |
| 4.2 | 0.000000 | 0.000000 |
| 4.3 | 0.000000 | 0.000000 |
| 4.4 | 0.000000 | 0.000000 |
| 4.5 | 0.000000 | 0.000000 |
| 4.6 | 0.000000 | 0.000000 |
| 4.7 | 0.000000 | 0.000000 |
| 4.8 | 0.000000 | 0.000000 |
| 4.9 | 0.000000 | 0.000000 |
| 5.0 | 0.000000 | 0.000000 |
| 5.1 | 0.000000 | 0.000000 |
| 5.2 | 0.000000 | 0.000000 |
| 5.3 | 0.000000 | 0.000000 |
| 5.4 | 0.000000 | 0.000000 |
| 5.5 | 0.000000 | 0.000000 |
| 5.6 | 0.000000 | 0.000000 |
| 5.7 | 0.000000 | 0.000000 |
| 5.8 | 0.000000 | 0.000000 |
| 5.9 | 0.000000 | 0.000000 |
| 6.0 | 0.000000 | 0.000000 |
| 6.1 | 0.000000 | 0.000000 |
| 6.2 | 0.000000 | 0.000000 |
| 6.3 | 0.000000 | 0.000000 |
| 6.4 | 0.000000 | 0.000000 |
| 6.5 | 0.000000 | 0.000000 |
| 6.6 | 0.000000 | 0.000000 |
| 6.7 | 0.000000 | 0.000000 |
| 6.8 | 0.000000 | 0.000000 |
| 6.9 | 0.000000 | 0.000000 |
| 7.0 | 0.000000 | 0.000000 |
| 7.1 | 0.000000 | 0.000000 |
| 7.2 | 0.000000 | 0.000000 |
| 7.3 | 0.000000 | 0.000000 |
| 7.4 | 0.000000 | 0.000000 |
| 7.5 | 0.000000 | 0.000000 |
| 7.6 | 0.000000 | 0.000000 |
| 7.7 | 0.000000 | 0.000000 |
| 7.8 | 0.000000 | 0.000000 |
| 7.9 | 0.000000 | 0.000000 |
| 8.0 | 0.000000 | 0.000000 |
| 8.1 | 0.000000 | 0.000000 |
| 8.2 | 0.000000 | 0.000000 |
| 8.3 | 0.000000 | 0.000000 |
| 8.4 | 0.000000 | 0.000000 |
| 8.5 | 0.000000 | 0.000000 |
| 8.6 | 0.000000 | 0.000000 |
| 8.7 | 0.000000 | 0.000000 |
| 8.8 | 0.000000 | 0.000000 |
| 8.9 | 0.000000 | 0.000000 |
| 9.0 | 0.000000 | 0.000000 |
| 9.1 | 0.000000 | 0.000000 |

[illegible]

[illegible]

```
TIME ,HCURS = 5.00000 .
```

LENGTH OF SOIL PROFILE, CM = 33.1250
VOLUME OF WATER IN THE SOIL PROFILE, CM = 11.16707

| | | | | |
|-------|------|----------|----------------------|-----------|
| TOTAL | NH-4 | IN EXCH. | PHASE, MG = | 46.63972 |
| TOTAL | NH-4 | IN SOIL | SOLUTION PHASE, MG = | 104.43523 |
| TOTAL | NH-4 | IN SCIL. | MG = | 151.07515 |

TOTAL N_P-3 IN SOIL SOLUTION, MG = 243.00962
 TOTAL ORGANIC N IN THE SOIL, MG = 1056.96265
 TOTAL N_C-2 RELEASED FROM THE SOIL, MG = 0.0

| DEPTH, CM | SUCTION, CM | THETA | HYDR. COND. | WATER FLUX | NH4 | NO3 | CORGN | NO2 |
|-----------|-------------|---------|-------------|------------|------------|------------|---------|-----|
| 0.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.1153E | 0.3721E-03 | 0.1983E | 0.0 |
| 0.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.2063E-01 | 0.6212E-03 | 0.1983E | 0.0 |
| 0.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.3009E-01 | 0.9681E-03 | 0.1983E | 0.0 |
| 0.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.3903E-01 | 0.1411E-02 | 0.1984E | 0.0 |
| 0.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.4703E-01 | 0.1948E-02 | 0.1984E | 0.0 |
| 0.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.5669E-01 | 0.2576E-02 | 0.1984E | 0.0 |
| 0.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.6533E-01 | 0.3224E-02 | 0.1984E | 0.0 |
| 0.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.7394E-01 | 0.4106E-02 | 0.1984E | 0.0 |
| 0.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.8222E-01 | 0.4992E-02 | 0.1984E | 0.0 |
| 0.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.9048E-01 | 0.5888E-02 | 0.1984E | 0.0 |
| 1.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.9861E-01 | 0.6792E-02 | 0.1984E | 0.0 |
| 1.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.1065E | 0.7702E-02 | 0.1984E | 0.0 |
| 1.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.1232E | 0.8616E-02 | 0.1984E | 0.0 |
| 1.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.1414E | 0.9532E-02 | 0.1984E | 0.0 |
| 1.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.1602E | 0.1058E-01 | 0.1984E | 0.0 |
| 1.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.1796E | 0.1205E-01 | 0.1984E | 0.0 |
| 1.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.1996E | 0.1349E-01 | 0.1984E | 0.0 |
| 1.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.2202E | 0.1501E-01 | 0.1985E | 0.0 |
| 1.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.2414E | 0.1660E-01 | 0.1985E | 0.0 |
| 1.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.2632E | 0.1827E-01 | 0.1985E | 0.0 |
| 2.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.2856E | 0.2002E-01 | 0.1985E | 0.0 |
| 2.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.3086E | 0.2184E-01 | 0.1985E | 0.0 |
| 2.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.3322E | 0.2372E-01 | 0.1985E | 0.0 |
| 2.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.3564E | 0.2572E-01 | 0.1985E | 0.0 |
| 2.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.3812E | 0.2776E-01 | 0.1985E | 0.0 |
| 2.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.4066E | 0.2977E-01 | 0.1985E | 0.0 |
| 2.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.4326E | 0.3172E-01 | 0.1985E | 0.0 |
| 2.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.4592E | 0.3372E-01 | 0.1985E | 0.0 |
| 2.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.4864E | 0.3577E-01 | 0.1985E | 0.0 |
| 2.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.5142E | 0.3777E-01 | 0.1985E | 0.0 |
| 3.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.5426E | 0.3972E-01 | 0.1985E | 0.0 |
| 3.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.5716E | 0.4172E-01 | 0.1985E | 0.0 |
| 3.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.6012E | 0.4372E-01 | 0.1985E | 0.0 |
| 3.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.6314E | 0.4572E-01 | 0.1985E | 0.0 |
| 3.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.6622E | 0.4772E-01 | 0.1985E | 0.0 |
| 3.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.6936E | 0.4972E-01 | 0.1985E | 0.0 |
| 3.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.7256E | 0.5172E-01 | 0.1985E | 0.0 |
| 3.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.7582E | 0.5372E-01 | 0.1985E | 0.0 |
| 3.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.7914E | 0.5572E-01 | 0.1985E | 0.0 |
| 3.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.8252E | 0.5772E-01 | 0.1985E | 0.0 |
| 4.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.8596E | 0.5972E-01 | 0.1985E | 0.0 |
| 4.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.8946E | 0.6172E-01 | 0.1985E | 0.0 |
| 4.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.9302E | 0.6372E-01 | 0.1985E | 0.0 |
| 4.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 0.9664E | 0.6572E-01 | 0.1985E | 0.0 |
| 4.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.0032E | 0.6772E-01 | 0.1985E | 0.0 |
| 4.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.0406E | 0.6972E-01 | 0.1985E | 0.0 |
| 4.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.0786E | 0.7172E-01 | 0.1985E | 0.0 |
| 4.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.1172E | 0.7372E-01 | 0.1985E | 0.0 |
| 4.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.1564E | 0.7572E-01 | 0.1985E | 0.0 |
| 4.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.1962E | 0.7772E-01 | 0.1985E | 0.0 |
| 5.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.2366E | 0.7972E-01 | 0.1985E | 0.0 |
| 5.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.2776E | 0.8172E-01 | 0.1985E | 0.0 |
| 5.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.3192E | 0.8372E-01 | 0.1985E | 0.0 |
| 5.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.3614E | 0.8572E-01 | 0.1985E | 0.0 |
| 5.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.4042E | 0.8772E-01 | 0.1985E | 0.0 |
| 5.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.4476E | 0.8972E-01 | 0.1985E | 0.0 |
| 5.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.4916E | 0.9172E-01 | 0.1985E | 0.0 |
| 5.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.5362E | 0.9372E-01 | 0.1985E | 0.0 |
| 5.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.5814E | 0.9572E-01 | 0.1985E | 0.0 |
| 5.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.6272E | 0.9772E-01 | 0.1985E | 0.0 |
| 6.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.6736E | 0.9972E-01 | 0.1985E | 0.0 |
| 6.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.7206E | 0.1017E | 0.1985E | 0.0 |
| 6.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.7682E | 0.1037E | 0.1985E | 0.0 |
| 6.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.8164E | 0.1057E | 0.1985E | 0.0 |
| 6.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.8652E | 0.1077E | 0.1985E | 0.0 |
| 6.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.9146E | 0.1097E | 0.1985E | 0.0 |
| 6.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 1.9646E | 0.1117E | 0.1985E | 0.0 |
| 6.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.0152E | 0.1137E | 0.1985E | 0.0 |
| 6.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.0664E | 0.1157E | 0.1985E | 0.0 |
| 6.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.1182E | 0.1177E | 0.1985E | 0.0 |
| 7.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.1706E | 0.1197E | 0.1985E | 0.0 |
| 7.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.2236E | 0.1217E | 0.1985E | 0.0 |
| 7.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.2772E | 0.1237E | 0.1985E | 0.0 |
| 7.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.3314E | 0.1257E | 0.1985E | 0.0 |
| 7.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.3862E | 0.1277E | 0.1985E | 0.0 |
| 7.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.4416E | 0.1297E | 0.1985E | 0.0 |
| 7.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.4976E | 0.1317E | 0.1985E | 0.0 |
| 7.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.5542E | 0.1337E | 0.1985E | 0.0 |
| 7.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.6114E | 0.1357E | 0.1985E | 0.0 |
| 7.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.6692E | 0.1377E | 0.1985E | 0.0 |
| 8.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.7276E | 0.1397E | 0.1985E | 0.0 |
| 8.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.7866E | 0.1417E | 0.1985E | 0.0 |
| 8.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.8462E | 0.1437E | 0.1985E | 0.0 |
| 8.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.9064E | 0.1457E | 0.1985E | 0.0 |
| 8.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 2.9672E | 0.1477E | 0.1985E | 0.0 |
| 8.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.0286E | 0.1497E | 0.1985E | 0.0 |
| 8.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.0906E | 0.1517E | 0.1985E | 0.0 |
| 8.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.1532E | 0.1537E | 0.1985E | 0.0 |
| 8.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.2164E | 0.1557E | 0.1985E | 0.0 |
| 8.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.2802E | 0.1577E | 0.1985E | 0.0 |
| 9.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.3446E | 0.1597E | 0.1985E | 0.0 |
| 9.1 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.4096E | 0.1617E | 0.1985E | 0.0 |
| 9.2 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.4752E | 0.1637E | 0.1985E | 0.0 |
| 9.3 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.5414E | 0.1657E | 0.1985E | 0.0 |
| 9.4 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.6082E | 0.1677E | 0.1985E | 0.0 |
| 9.5 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.6756E | 0.1697E | 0.1985E | 0.0 |
| 9.6 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.7436E | 0.1717E | 0.1985E | 0.0 |
| 9.7 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.8122E | 0.1737E | 0.1985E | 0.0 |
| 9.8 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.8814E | 0.1757E | 0.1985E | 0.0 |
| 9.9 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 3.9512E | 0.1777E | 0.1985E | 0.0 |
| 10.0 | 0.0 | 0.3588E | 0.3227E | 0.4115E | 4.0216E | 0.1797E | 0.1985E | 0.0 |

[illegible]

[illegible]

[illegible]

TIME = 10.0000
LENGTH OF SCIPROFILE = 10.0000
CM = 10.0000

VOLUME OF WATER IN THE SOIL PROFILE, CM = 17.271

TOTAL NH-4 IN EXCH. PHASE. MG = 34.68225

| TOTAL | IN SCIL | MG | IN SCIL | SOLUTION PHASE, |
|-------|---------|----------|---------|-----------------|
| 24-4 | 24-4 | 112.2593 | 24-4 | 24-4 |
| 24-4 | 24-4 | 112.2593 | 24-4 | 24-4 |
| 24-4 | 24-4 | 112.2593 | 24-4 | 24-4 |
| 24-4 | 24-4 | 112.2593 | 24-4 | 24-4 |

TOTAL NH-3 IN SCIL SOLUTION: MG = 288.06494
TOTAL ORGANIC N IN THE SOIL: MG = 1610.29150
TOTAL NC-2 RELEASED FROM THE SOIL: MG = 0.0